



GEOTECHNICAL COMPLETION REPORT STAGE 2

Lot 14 DP 374000 51 TE MAIKA ROAD, NGUNGURU

Job Details: Residential Subdivision – Stage Two

Job number: 20-0078
Client: Traverse Ltd

Site Address: 51 Te Maika Road, Ngunguru

Legal Description: Lot 14 DP 374000

Date: 16 August 2022
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Core Engineering Solutions Limited

Geotechnical Completion Report for Stage 2 - Residential Subdivision at Lot 14 DP 374000 51 Te Maika Road, Ngunguru

Job No	20-0078			
Project Name	Residential Subdivision – Stage Two			
Street Address	51 Te Maika Road, Ngunguru			
Legal Description	Lot 14 DP 374000			
Applicable Consents	SL2100003			
Client	Traverse Ltd			
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Version No	3			
Date	28/09/2022			
Author Signature				
Authoriser Signature				

Please note that NZS4431:1989 has been updated during the course of this project to NZS4431:2022.

This document refers to both NZS4431:1989 and NZS4431:2022. This is not an error and relates to the change in practices outlined in each of these documents and the timeframe during which earthworks took place.



1. INTRODUCTION

This Geotechnical Completion Report (GCR) has been prepared By Core Engineering Solutions Ltd (CES Ltd) for Traverse Ltd as part of the documentation to be submitted to Whangarei District Council (WDC) on completion of the Stage Two of the Te Maika Road subdivision in Ngunguru, located at 51 Te Maika Road, Ngunguru, hereinafter referred to as 'the site'. Stage Two initially comprises of the development of eight residential lots with the inclusion of Lot 33 (Balance Lot).

This report addresses the geotechnical engineering aspects of the subdivision development, identifies and discusses geotechnical engineering issues that must be taken into consideration during individual Lot development, and includes a Statement of Professional Opinion (SOPO) that covers the Suitability of the Land for its Intended Purpose. The SOPO includes a summary table, outlining the Geotechnical Design Recommendations from CES Ltd in regard to individual Residential Lots. The SOPO is located within Appendix One.

The subdivision design was prepared by Reyburn & Bryant Limited (R&B Ltd), and the main civil contractor was Clements Contractors Ltd (CC Ltd). Supporting Producer Statements for construction are included and appended to this report.

CES Ltd Drawings in this report are based on final contour levels provided by Reyburn and Bryant for the purposes of establishing building setbacks. Final 'AS Built' plans are to be provided by Reyburn and Bryant.

CES Ltd was commissioned to observe and undertake construction monitoring for earthworks and specific design engineering works (e.g. retaining walls).

Subdivision Earthworks were carried out in general accordance with NZS4404:2010 Land Development and Subdivision Infrastructure, NZS 4431:1989 and NZS4431:2022 Code of practice for Earth Fill for Residential Development.

This document has been prepared in general accordance with the Whangarei District Council (WDC) Engineering Standards 2022, with special reference to Site Development Suitability (Geotechnical and Natural Hazards).



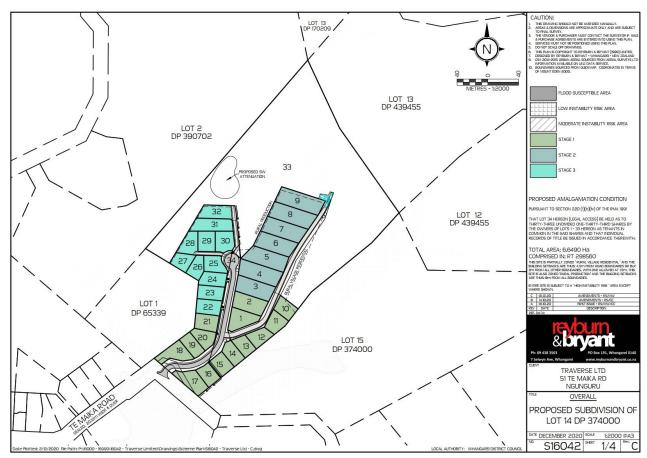


Figure 1 - Map of subdivision, showing various Stages. (Source R&B Ltd)

2. SITE DESCRIPTION

This 66490m² property is located on the northern side at the end of Te Maika Road. The property has a prominent broad crested spur ridgeline which runs down towards the south. The western and north-western boundaries back onto the flank of a ridgeline that runs through the neighbouring properties.

Stage Two of the Te Maika Road Development occupies the north eastern part of the property at 51 Te Maika Road Ngunguru, currently legally described as Lot 14 DP 374000. Flanks on the ridgeline generally ranged between 20° and 30°. Groundcover is grass within the low-lying areas. On the spur ridgeline, the allotments have been recently planted with native bush and shrubs located on the flanks.

The extent of Stage Two within this property is presented on the R&B 'Scheme Plan' drawings contained in Appendix 3. Stage Two Lots comprise the higher areas of the subdivision extending up the ridgeline, namely Lots 3-9 inclusive and Lot 33.



2.1 Completed Subdivision Works

The completed Stage Two Subdivision has resulted in the formation of eight new residential Lots (Lots 3-9 inclusive and Lot 33) that, on completion of the subdivision works and certification from Council, will be released for individual development.

2.2 Topographical Description Post-Construction

The land within Stage Two has undergone significant transformation in order to obtain the finished site profile. Stage Two sections level building sites, with sea and estuary views to the south.

Topsoil and non-engineered fill has been removed from the site. A significant volume of silt clay fill from the spur to the northeast of the site has been cut and transported down the hill to raise the valley and form the road and new platforms, mitigating the flood hazard and liquefaction risk. Residential Lots have been raised above flood heights and are more evenly sloping.

Roads and infrastructure have been constructed. Infrastructure includes stormwater, wastewater, power and internet (fibre) infrastructure. Topsoil has then be reinstated.

Stage Two sites are all created completely within cut (natural ground), and no settlement monitoring is required for these sites.

Fifteen retaining walls have been built within Stage Two of the subdivision, with two of the retaining walls located on the downhill (southern) side of Lot 3 within Stage One.

The finished site topography is to be supplied by Reyburn and Bryant with the As-Built plans. CES Ltd has been supplied finished levels over Stage 2 so that final setbacks and individual allotment recommendations can be provided.

3. PREVIOUS WORK

The following reports on this site have been previously issued:

- Engineering Report for Subdivision for the property by Richardson Stevens Consultants (1996) Ltd, Ref: 6886, dated: 5 November 2007 (Amended June 2008)
- Geotechnical Assessment Longview Estuary Estate Ngunguru (30 October 2007) Riley Consultants
- Subdivision Report 51 Te Maika Road Ngunguru (31 October 2018) Wilton Joubert Consulting Engineers Ref#81048, covering the original initial stage of this development (now known as Stage 2)



The following reports on this development have previously been issued by CES Ltd:

- Subdivision Report, Lot 14 DP 374000, 51 Te Maika Road Ngunguru (4/12/2020)
- Retaining Wall Design and Calculations (15/12/2020)
- Concrete Driveway reinforcing detail (20/05/2022)

4. SITE OPERATIONS

4.1 Construction Works and Programme

The primary works on-site were carried out between January 2021 and August 2022. Earthworks comprised:

- Cut and fill earthworks
- Installation of Geocomposite materials
- Retaining Wall structures construction
- Creation and relocation of main drain
- Fill old drain
- Construction of roads and services (power, telecommunications, stormwater and wastewater, sewers, firefighting tanks etc.)
- Topsoil spreading upon completion of the bulk formation and retaining wall construction works
- Planting of native seedlings to stabilise ridge flanks

Services such as stormwater, wastewater and firefighting tanks were constructed at the completion of earthworks. Refilling trenches and compaction of excavated areas was monitored by Clements Contractors Ltd.

Likewise, utility services (power, telecommunication etc,) were constructed following the completion of the bulk earthworks. Refilling trenches and compaction of excavated areas was monitored by Clements Contractors Ltd.

4.2 Extent of Formation Works

Stage Two was the source of fill for the balance of the subdivision. Areas of up to 8.0m in depths were excavated from the upper reaches of the hill in order to provide sufficient fill for the balance of the subdivision.

Stage Two land was affected by the site formation works, and final levels are to be supplied with the Reyburn and Bryant As-Built Plans.



4.3 Field Control

During the construction of the terraced retaining walls within this stage, excavated foundations were intermittently inspected as the walls were constructed to ensure that the ground conditions were in accordance with the design parameter. Site observations revealed that the retaining walls and building sites are well set into completely weathered greywacke. In-situ shear strengths were taken throughout the construction of these walls and were all well in excess of 140kPa (uncorrected). Foundations for these walls were up to 2.8m below cleared ground level with no signs of elevated groundwater. The recovered soil from the excavation of the foundations did not reveal any colour disfiguration or mottling to suggest a seasonal perched water table.

Calibrated Pilcon Shear Vanes, used in accordance with New Zealand Geotechnical Society Guideline for Hand Held Shear Vane Test, 2001, were used every 0.2m in the hand augered drilled holes, measuring both in situ and remoulded strengths.

At the completion of earthworks on the hill locations, samples of both cut parent material and fill at finished ground level were obtained from eleven locations across the entire subdivision and the material was sent to Geocivil in Whangarei for Atterberg Testing and linear shrinkage testing to assist with establishing the anticipated soil expansivity and classification. Results for this are appended.

Post-earthworks on-site testing was undertaken on the hill sites. DPSH-B testing was undertaken on the hill sites to establish depth to solid less weathered greywacke to assist with collating a profile of the underlying soil strata. DPSB-B testing indicated a consistent depth to hard material down the hill of between 14.6 and 18.0m BGL.

The tests above have been used in conjunction with the previous subsoil testing, our ongoing monitoring and observations to gain an understanding of the overall ground conditions within Stage 2.

5. EVALUATION OF SITE FOR RESIDENTIAL DEVELOPMENT

The majority of the lower areas of the subdivision have been raised using fill material harvested from Stage 2 of the Development. Earthworks have been carried out in such a manner as to form level or near level sites throughout the subdivision. The final levels within Stage 2 were not finalised until earthworks for Stage 1 and 3 were near complete. This was due to exact fill quantities being unknown as it was dependent on the extent of undercutting required over the lower areas of the site. Reyburn and Bryant Ltd have supplied the As-Built Plans finished heights over the entire development, and these are appended to this report.



CES Ltd considers Stage Two of this Development as largely free of significant geotechnical issues that would affect Lot development; however, specific items that may affect development within the subdivision are noted below.

5.1 General Ground Conditions

All residential Lots within Stage Two have been affected by undercutting, which has exposed the underlying completely weathered Waipapa Group geology (Greywacke). The excess cut material has been used as bulk fill to assist with constructing Stages 1 and 3 in general accordance with NZS4431:2022. This material has proven to be exceedingly consistent throughout the cut areas in Stage 2 and with Linear Shrinkage ranging from 13 to 19.

Stage 2 is completely situated in areas that were subject to bulk excavation (cut), and thus, underlying in situ soils were exposed in these locations prior to topsoil respreading.

5.2 Seismic Classification

The development is proposed to include residential dwellings and supporting structures which are assessed to be, as a minimum, designed to be an Importance level 2 (IL2) structure in accordance with NZS1170. Return periods for limit state design events for an IL2 structure are Serviceability Limit State (SLS) 1/25 years and Ultimate Limit State (ULS) 1/500 years.

CES Ltd undertook an assessment of the Seismic Subsoil Class, as per the criteria outlined in NZS 1170.5. Soils on-site demonstrated stiff and very stiff representative undrained shear strengths, at depths of less than 20m.

CES Ltd assesses the site subsoil class as being a Class C – Shallow Soils Site in accordance with Section 3.1.3, NZS1170.5.

5.3 Liquefaction

Reference has been made to the 2017 Geotechnical Modules released by MBIE, EQC and the Ministry for the Environment, Planning and Engineering Guidance for potentially liquefaction-prone land. Previous assessment in regard to liquefaction has been addressed by CES Ltd at the initial application stage for this development (Refer to CES Ltd Subdivision Report as referenced under Section 3 of this report).

Stage Two of the Te Maika Road subdivision has been assessed by CES Ltd on the following basis:

- Deep groundwater levels, groundwater >4.0m.
- Any uncontrolled fill has been removed.
- Clear of geologically young OIS1 (Holocene) river deposits.
- Clear of swamp areas with elevated groundwater levels.



This subdivision lies within an area of the country with a low seismicity risk. In our opinion, CES Ltd is satisfied that the risk of liquefaction within Stage 2 of this development is low.

5.4 Expansive Soils

The underlying soil within this development stage comprises of completely to highly weathered Waipapa Group. Experience with similar soils elsewhere suggests that the site soils are likely to be susceptible to seasonal shrink/swell movements as the ground dries out and then wets up in a cyclic manner from summer to winter. However, it is more common that the upper residual soils are typically more susceptible to shrinkage and swelling, and with this material removed from the sites within Stage 2, expansive soils are expected to be less variable.

The New Zealand Building code defines 'good ground' in the following manner:

'Good ground means any soil or rock capable of permanently withstanding an ultimate bearing pressure of 300 kPa (i.e. an allowable bearing pressure of 100 kPa using a factor of safety of 3.0), but excludes:

- a) Potentially compressible ground such as topsoil, soft soils such as clay which can be moulded easily in the fingers, and uncompacted loose gravel which contains obvious voids,
- b) Expansive soils being those that have a liquid limit of more than 50% when tested in accordance with NZS 4402 Test 2.2, and a linear shrinkage of more than 15% when tested, from the liquid limit, in accordance with NZS 4402 Test 2.6, and
- c) Any ground which could foreseeably experience movement of 25 mm or greater for any reason including one or a combination of: land instability, ground creep, subsidence, liquefaction, lateral spread, seasonal swelling and shrinking, frost heave, changing ground water level, erosion, dissolution of soil in water, and effects of tree roots.

CES Ltd identified the soils as expansive in our initial site investigations stage and proposed to defer classification until earthworks completion. Since soils are expansive in nature, and the foreseeable movement is expected to be greater than 25mm, therefore soils on-site are not considered to meet the definition prescribed above for 'good ground'.

CES Ltd commissioned Geocivil Ltd to undertake Linear Shrinkage testing and determination of the liquid limit, plastic limit, plasticity index and water content from samples of the Waipapa Group parent material and of the material placed as fill. This form of testing was preferred due to the geology present.

The samples taken in within stage were retrieved from within the cut ground (~4.0m below natural ground level) on Lot 4, Lot 7 and Lot 33 (Sample 1). The samples returned a Plasticity Index (PI) ranging between 23 and 44. The Liquid Limit (LL) ranged from 55 to 83. Linear shrinkage (LS) testing of the sample taken resulted in a LS ranging from 13% and 17%.

In NZS 3604:2011, expansive soils are defined as those with:



- Liquid Limit, LL > 50% (as tested by NZS4402.2.2:1986)
- Linear Shrinkage, LS > 15% (as tested by NZS4402.2.6:1986)

From the sample taken on the ridgeline, and the above criteria for expansive soils, we are satisfied that the soils on-site are expansive in nature as the liquid limits exceed the definition above. From further review of the results and use of the Casagrande Plasticity Chart, the soils on-site are assessed as a elastic SILT which exhibits low to medium levels of plasticity. The linear shrinkage results were marginally over the threshold for 'good ground' in accordance with NZS3604, therefore soil expansivity of higher than a CLASS S as per NZBC – B1 should be expected.

From the above and experience with the geology present at the site, CES Ltd assesses the soils onsite for this stage of the subdivision as Class M – Moderately Expansive in accordance with NZBC – B1 Structure.

5.5 Settlement Monitoring

Stage Two of the Te Maika Road Subdivision has been completely created within cut. No settlement monitoring is required within Stage Two of this subdivision.

5.6 Bearing Capacity

Post earthworks subsoil testing, including visual inspection and shear vane testing of cut soils and DPSH-B testing over Stage 2, revealed soils which were very stiff and dry along the ridgeline.

Dynamic Probe Super Heavy – B type testing (DPSH-B) involves driving a 20cm² probe into the ground using a 63.5kg hammer dropping 760mm. Penetration is recorded as the number of hammer drops per 200m penetration by the probe.

The test methodology therefore is similar to a Standard Penetrometer Test (SPT), utilising the same sized hammer and drop. The SPT utilises a split spoon sampler, bringing samples to the surface, whereas no samples can be recovered using DPSH-B.

DPSH-B tests were driven until effective refusal – CES Ltd term effective refusal as anything greater than 30 blows per 200mm penetration. DPSH-B results are appended to this report.

Shallow shear vanes (finished ground level) and deeper shear vanes (retaining pile holes) were taken at numerous locations across Stage Two sites. Results indicated a high (consistently >100kPa) shear strength is available at both shallow and deeper depths.

Three Hand Augered boreholes were undertaken On Lot 3, Lot 6 and Lot 9. Borehole results are appended to this report.



CES Ltd assesses that the soils at each proposed building site will achieve an Ultimate Bearing Strength of 300kPa from below cleared ground level. As required by the Building Code, a strength reduction factor must be applied to the above values in order to determine the dependable values for use in ultimate limit state design; a reduction factor of 0.5 is recommended.

When considering the above and ignoring the topsoil layer, near-surface soils (within 2m of finished ground levels) within each building platform are generally considered to comply with the requirements of NZS3604:2011 and, with the exception of expansive soil properties, should otherwise be designated as 'good ground'.

5.7 Lot Gradients & Stability

Within Stage Two, the majority of residential Lots have been finished with a near level or gently sloping gradient. All lots have a steep slope to the west. Rihi Paea Rise is on the eastern side of the sections, and there is a batter down to Rihi Paea Rise from each of the sections. Lot 3 to Lot 9 are finished with terraced retaining walls present to the north and south of each of the Lots.

Lot 33 contains the balance of land leftover from the subdivision. A building platform has been constructed at the top of the hill for Lot 33, on the top of the ridge. There is a retaining wall at the base Lot 33 at the boundary with Lot 9. A site-specific geotechnical assessment and foundation design will be required for the dwelling on Lot 33.



Figure 2 - Lot 1 and Lot 2 during the construction phase. Note the location of the retaining walls and batters on the left and right-hand sides (west and east). Source CES Ltd.

Pre-development slope stability analysis, as discussed in reports listed in Section 3, suggested that the site profile would remain stable post-earthworks. However, as final levels were not known, a



further assessment of the setback requirement to the flanks and retaining structures was deferred to the earthworks completion stage. CES Ltd has undertaken an assessment of the flanks to ascertain a suitable setback from the slopes in accordance with WDC – Land Development Stabilisation – Technical Design Requirements Policy (Dated: April 2018).

5.7.1 Subsoil Conditions

The flank slopes did not indicate any signs of previous instability and are standing at grades of up to 25 degrees. Cut faces within this stage were left near vertical and exposed by the contractor for the majority of the 2021 winter period. No signs of significant slippages occurred, which provided confidence that the recently exposed, completely weathered material is consistent at depth. DPSH-B testing confirmed the depth to the underlying moderately weathered greywacke.

Due to the lack of evidence of slope failure on the slopes a back analysis was not undertaken and the reliance on parameters used are based on experience with this geology in the area.

5.7.2 Groundwater Conditions

Groundwater has been conservatively assumed to be as shallow as 1.0m below finished ground level for the elevated groundwater level and as shallow as 2.0m below finished ground level at the lower end of the flank for normal groundwater levels.

5.7.3 Site Seismic Characteristics

Ground motion inputs from Table A1 of the NZGS/MBIE Earthquake Geotechnical Engineering Practice Module 1 have been adopted for the purpose of geotechnical engineering assessment within this report. Due to the location of the site, Method 1 of the Module 1 has been adopted to determine the Peak Ground Acceleration (PGA). From Appendix 1 of Module 1, a conservative approach has been taken, and we have adopted the PGA for a 500-year return period of 0.19. This PGA is to be adopted for stability assessment of the ridge flanks.

Module 6 of the MBIE guidance documents has been adopted to calculate the horizontal design acceleration with the position of the building and retaining structures in relation to slopes down the ridgeline as generally considered to be a Class 3 scenario with a Topographical factor of 1.0 and wall displacement factor of 0.5. Based on these guidelines, a minimum PGA for pseudo-static design of 0.095 has been adopted for down the ridgeline where retaining structures have been constructed.



Results of this updated stability analysis are summarised within Appendix 7. From the analysis, CES Ltd is satisfied that a stable building site is available on each allotment, provided compliance with this report. A minimum building setback of 3.0m to the flanks is to be applied to the building sites and upper level areas of the existing retaining structures without further stability assessment by a geo-professional.

5.8 Retaining Walls

As indicated on the CES Ltd plans (Refer to Appendix 4), fifteen retaining walls have been constructed within or adjacent to Stage Two to form level or gently sloping building platforms on Lots 3-9.

Retaining walls were built to the CES Ltd design (Appendix 4).

Retaining walls have been designed assuming a surface surcharge value of 2.5kPa above each wall. These retaining walls have been designed to accommodate loadings generated by lightweight vehicles (as defined in NZS1170) and does not consider any permanent loads in close proximity to the walls. A minimum setback of 3.0m horizontally from the upper walls will need to be maintained from any structures to avoid any additional surcharge loads.

Alternatively, specific design advice should be sought from a suitably qualified Chartered Professional Engineer should any structure or foundations be designed to intrude into this setback area.

It is recommended that only limited site formation works take place immediately in front (downslope) of any retaining walls. Any works that require excavation greater than 0.5m deep should be subject to a specific engineering design to ensure that retaining walls are not undermined. Further to this, it is recommended that a minimum setback of 1.5m from the downslope retaining wall be applied for any future development. To illustrate the building setback, a 'Restricted Development Area Plan' has been prepared by CES Ltd and is appended to this report, refer to Appendix 4. Restricted Development Areas are discussed in further detail within Section 5.12 below.

5.9 Piped Services, Service Trenches and Drainage

As indicated within the approved engineering plans for the development, council stormwater and sewer reticulation are present. In general, these services are either constructed within road reserves or adjacent to Lot boundaries. As such, we consider it unlikely that such constructed services would be encountered during individual Lot development. Regardless, all building works on individual Lots should be laid out so as not to disturb any nearby services.



Should any site-specific development layouts that encroach near or over these services be unavoidable, foundations must be designed per current WDC Engineering Standards guidelines for building near or over services (WDC Policy #0022).

5.10 Topsoil

Topsoil depths were checked on individual Lots. The topsoil check indicated variable topsoil thicknesses, ranging from 100mm to 300mm. An average thickness of approximately 150mm is anticipated across the subdivision.

5.11 Stormwater Control

A stormwater reticulation system servicing the subdivision was constructed as part of the site formation works. All stormwater run-off from hard-standing areas (driveways, patios, footpaths etc) and any outflow from rainwater tank overflow, should be directed towards the stormwater system for disposal.

On-site stormwater disposal or soakage systems are not recommended unless further site-specific assessment is undertaken by a suitably qualified and experienced engineer. Under no circumstances should stormwater be disposed of by allowing it to flow onto or into the ground in an uncontrolled manner at any location on the subdivision.

5.12 Restricted Development Areas

From the assessment above, Restricted Development Areas have been imposed on portions of Stage Two, specifically Lot 3-9 and Lot 33.

These Restricted Development Areas have been imposed due to:

- Flanks on the ridgeline being in excess of 20 degrees (Lot 3-9 and Lot 33)
- Downslope of a retaining wall within 1.5 times the overall height of the wall (Lots 3-9)

Any developments that encroach on into a Restricted Development Area will need to be subject to a specific engineering investigation and design at the Building Consent stage. This is to ensure that future developments will not have an adverse effect on slope stability or retaining wall stability.

Lot 33 has a large area in comparison to the other allotments within Stage 2. It is proposed that any future structures within this allotment require a site-specific geotechnical assessment to accompany any Building Consent application.

For reference, CES Ltd has prepared a site plan outlining and summarising areas suitable for residential development and recommendations within Appendix 2 and 4 of this report.



Lots within Stage 2 are characterized by retaining walls above and below the Lots. No modification should be undertaken to retaining walls should be undertaken without consultation with a Chartered Professional Engineer familiar with the site.

Likewise, there are significant batter slopes present to the east and west of the Lots. Slope and batter modification, including low retaining walls, should only be undertaken after consultation with a geo-professional familiar with the site.

6. CONCLUSION

From our assessment of the site and construction monitoring, CES Ltd is satisfied that the proposed new allotments with Stage 2 are suitable for residential development, designed in general accordance with NZS:3604. A summary of each site is appended to this report for referral for site-specific developments. This report is intended to provide design guidance for the future development of the individual allotments. Should any works deviate from the recommendations of this report, then a site-specific assessment by a Geo-Professional (as defined within the WDCEES) should be undertaken prior to application for Building Consent.

A summary of the site restrictions are as follows;

Lots 3 - 9

- Buildings are to be setback a minimum of 3.0m from the ridgeline flanks and existring retaining structures within the development. Should any site specific development on the site encouch into this setback an assessment by a geo-professional should be undertaken to ensure the site stability.
- A minimum setback of 1.5m from the downslope retaining wall be applied for any future development infront of the existing retaining walls.
- Any developments that encroach on into a Restricted Development Area will need to be subject to a specific engineering investigation and design at the Building Consent stage.
- Foundations will need to be designed for Class M Moderately Expansive in accordance with NZBC B1 Structure.
- All stormwater run-off from hard-standing areas (driveways, patios, footpaths etc) and any outflow from rainwater tank overflow, should be directed towards the stormwater system for disposal.
- On-site stormwater disposal or soakage systems are not recommended unless further sitespecific assessment is required by a suitably qualified and experienced engineer.

Lot 33

- Any future structures within this allotment require a site-specific geotechnical assessment to accompany any Building Consent application



7. APPENDICES

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APPENDIX 1 – STATEMENT OF PROFESSIONAL OPINION

Job No: 20-0078

Statement of Professional Opinion on Suitability of Land for Building Construction

		Development	Traverse Ltd - Te Maika Road Development
		Developer	Traverse Ltd
		Location	51 Te Maika Road, Ngunguru, Whangarei
		I (full name)	David Andrew Leslie
	Of (Nar	me and address of firm)	Core Engineering Solutions Ltd, 31 Vine Street Whangarei
1	and w		onal as defined in Section 1.3 Abbreviations and Definitions ne Developer as the geo-professional on the above
2	Subdi —Ref:2 of that The ex	vision Report _ date to-0078 _ date t/those documen extent of my inspe- ations carried ou	minary investigations are described in my Report(s) number edRev 01 21/05/2021 and the conclusions and recommendations at(s) have been re-evaluated in the preparation of this report. ections during construction, and the results of all tests and/or retare as described in my geotechnical completion report dated
3	•	professional opi propriate):	nion, not to be construed as a guarantee, I consider that (delete
	a.	placed in comp Council and my 10-12 (Stage 1), 29-32 (S	shown on the attached Plan Nohave been bliance with the requirements of the Whangārei District y specification. (However, lots did not pass final fill esting and as a result, specific site investigations and
		-	igns will be required here at the time of building consent
	b.	considerations earthworks res	works take into account land slope and foundation stability, subject to the appended foundation recommendations and trictions, (which should be read in conjunction with the site contour plan)
	C.	satisfies the de	and 3(b) above, the original ground not affected by filling escription of 'good ground' as described in B1 Acceptable Verification Methods and NZS 4229:2013
/H	no a sr	pecific foundation	n investigation/design will be required at the time of Building

(If no, a specific foundation investigation/design will be required at the time of Building Consent)

d. Subject to 3(a) and 3(b) above, the filled ground satisfies the description of 'good ground' as described in NZS 3604:2011 and NZS 4229:2013 ☐ Yes X

(If no, a specific foundation investigation/design will be required at the time of Building Consent)

e. The original ground not affected by filling and the filled ground are not subject to erosion, subsidence, or slippage in accordance with the

	that:
i.	Compliance with the Subdivison Report and Geotechnical Completion Reports by CES Ltd for this development.
 ii.	Vibrations and Land Excavations within Stage 1 and 3 for site specific developements, are
	overseen and undertaken in responsible manner by suitably experienced contractors.
iii.	
iv.	
4	This professional opinion is furnished to the TA and the Developer for their purposes alone on the express condition that it will not be relied upon by any other person and does not remove the necessity for the normal inspection of foundation conditions at the time of erection of any building
5	This certificate shall be read in conjunction with my geotechnical report referred to in clause 2 above and shall not be copied or reproduced except in conjunction with the full geotechnical completion report
	BEng(Civil), DipEng(Civil), MEMgt(Hons) CMENGNZ, CPEng(Geotechnical/Structural) 16/08/2022

Professional Qualifications

Date

provisions of section 106 of the Resource Management Act 1991 provided

Signature



APPENDIX 2 – SUMMARY OF GEOTECHNICAL DESIGN RECOMMENDATIONS

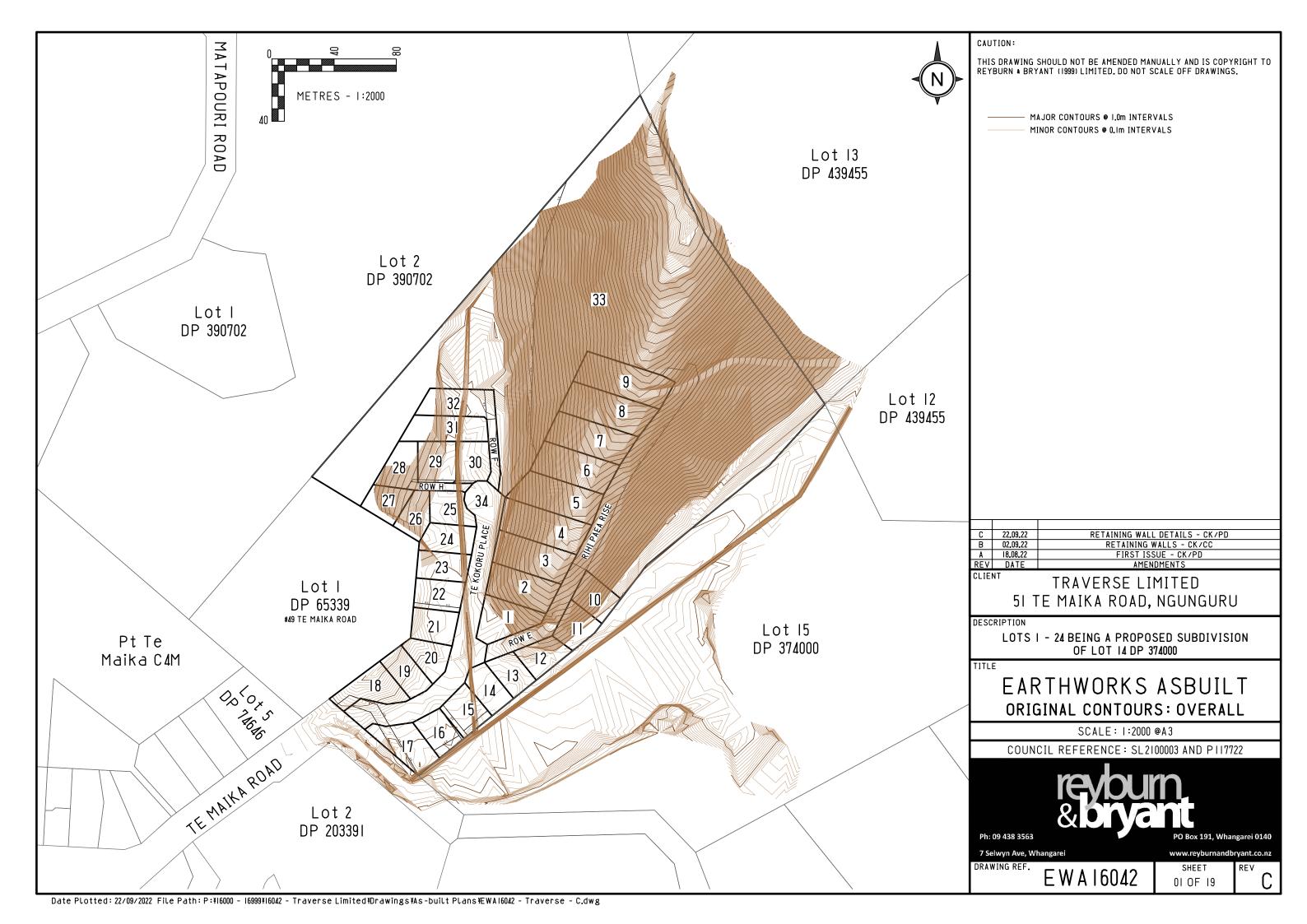
Job No: 20-0078

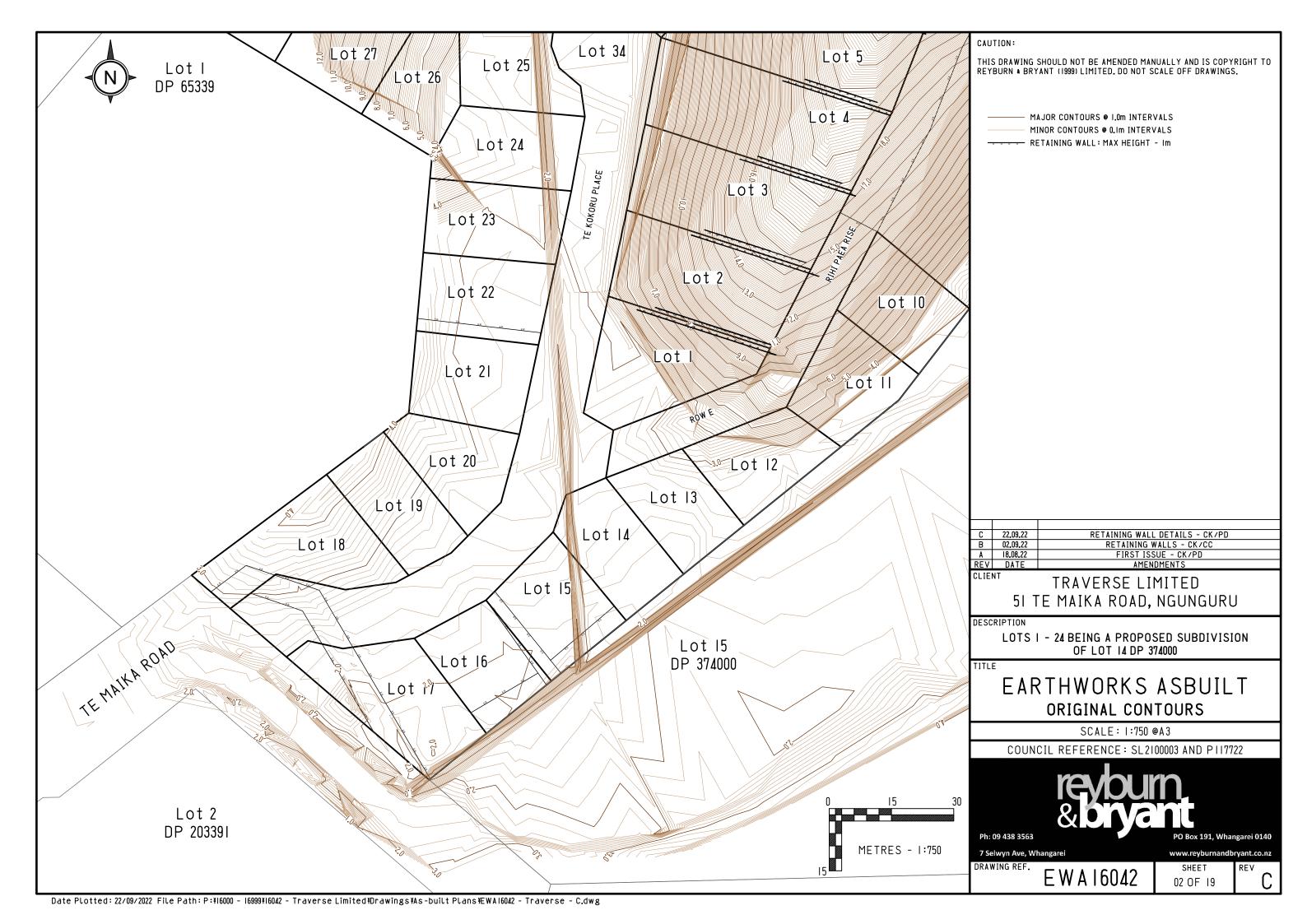
Lot No	Area	Anticipated Soil Type	Unworked Natural Ground Present within Lot	Foundations may be designed to 3604:2011	Shallow Foundations Ultimate Unfactored Bearing Capacity	Expansive Soils Present	Site Soil Classification (as defined in NZBC - B1)	Resticted Development Area Present on Lot	Other Comments
	m²	Fill	Y/N	Y/N	(kPa)	Y/N	(S, M, H, E)	Y/N	
3	1043	In Situ Soil	Υ	No, SED Design to account for expansive soils required for buildings within setback lines	300	Υ	М		
4	1169	In Situ Soil	Υ		300	Υ	М		
5	1147	In Situ Soil	Υ		300	Υ	М		
6	1065	In Situ Soil	Y		300	Y	М	Yes, minimum setback from retaining wall structures and flanks as defined in Appendix 4 of the GCR, any works	Any development outside of the building restrictions will require further investigations by a suitably
7	1108	In Situ Soil	Υ		300	Υ	М	within these setback will require further review by a Geo-professional	qualified engineer in accordance with WDCEES 2022
8	1186	In Situ Soil	Υ		300	Υ	М		
9	1249	In Situ Soil	Υ		300	Υ	М		
33	39146	In Situ Soil	Y		300	Y	М		

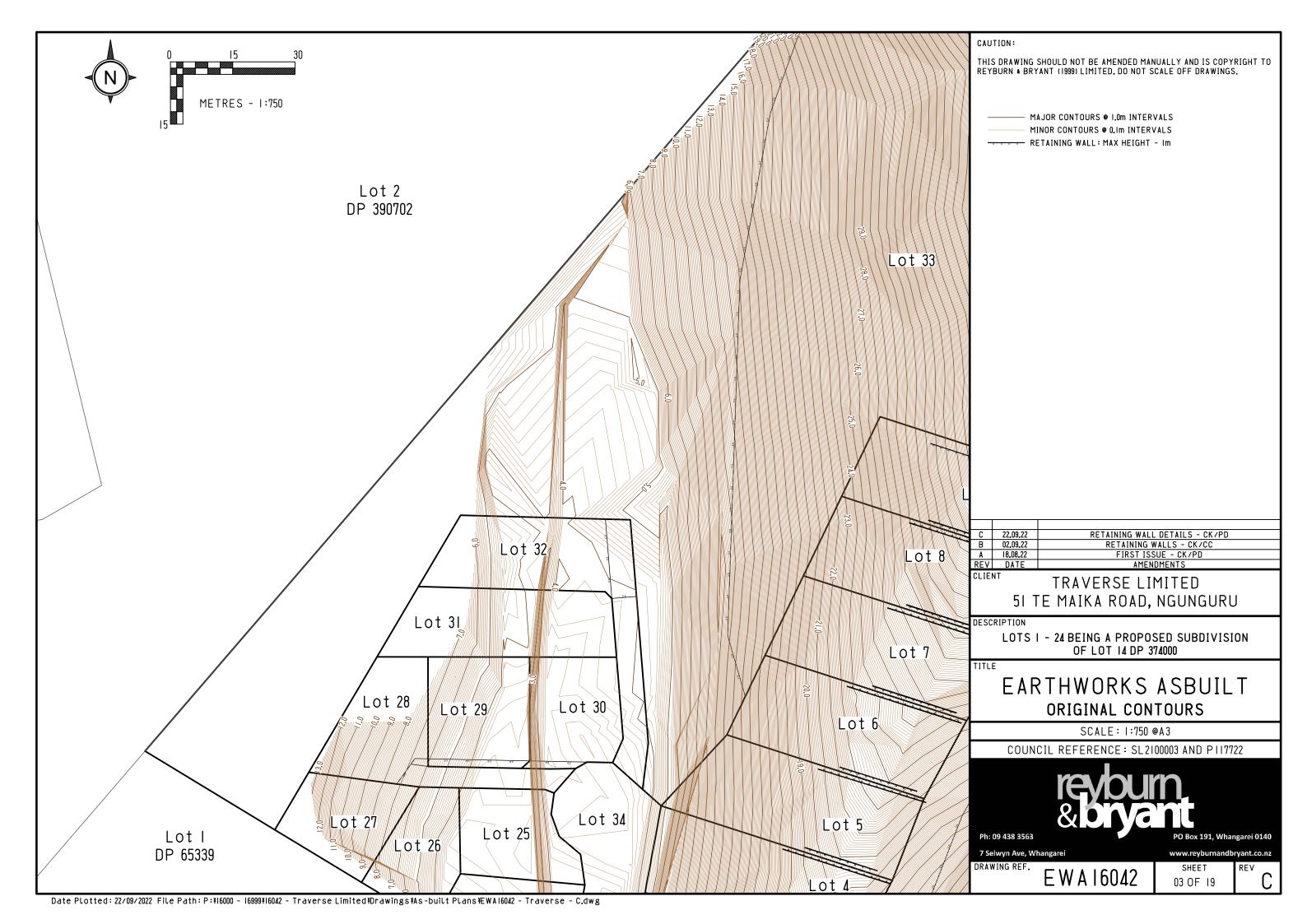


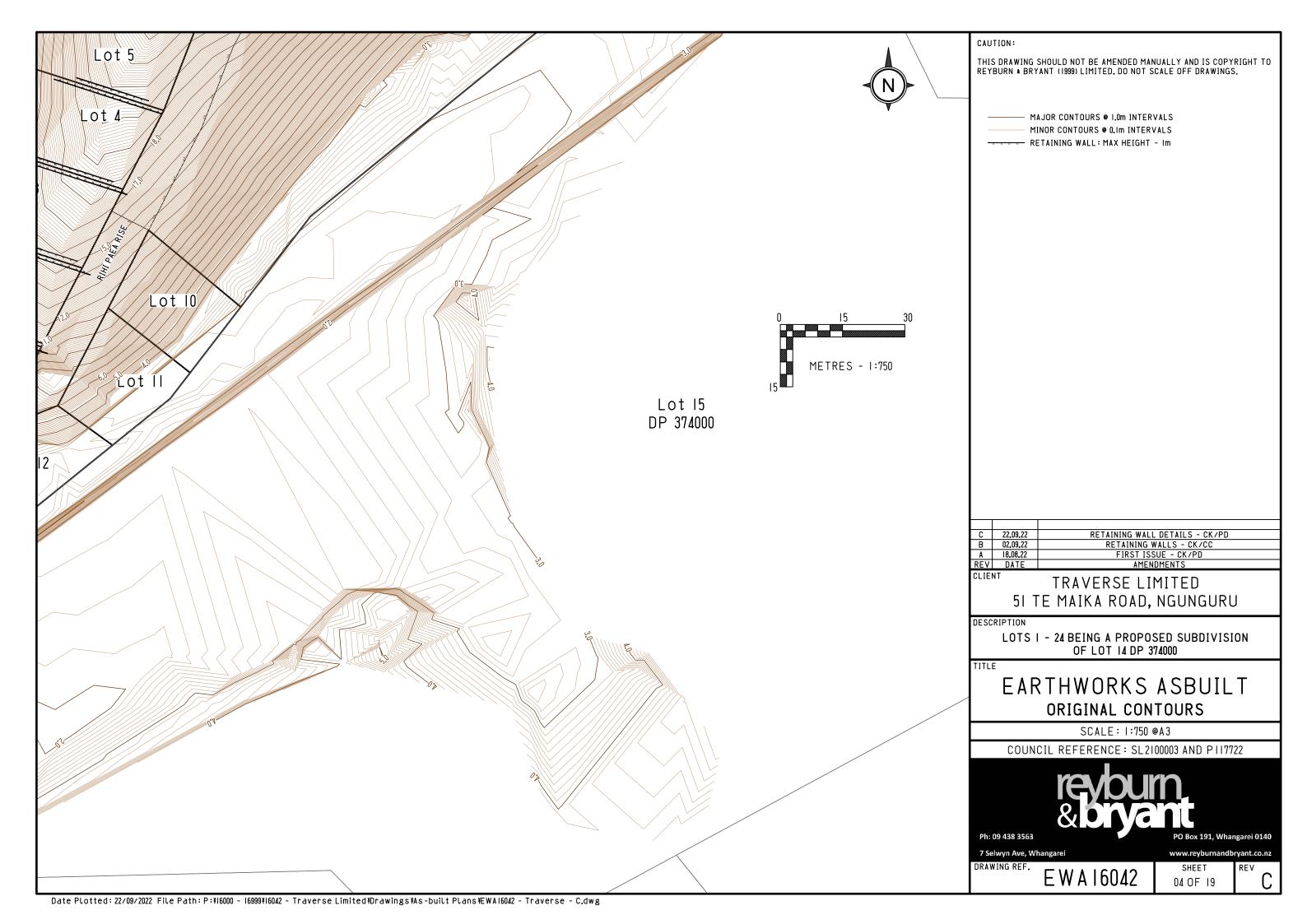
APPENDIX 3 - REYBURN & BRYANT LTD SCHEME PLAN

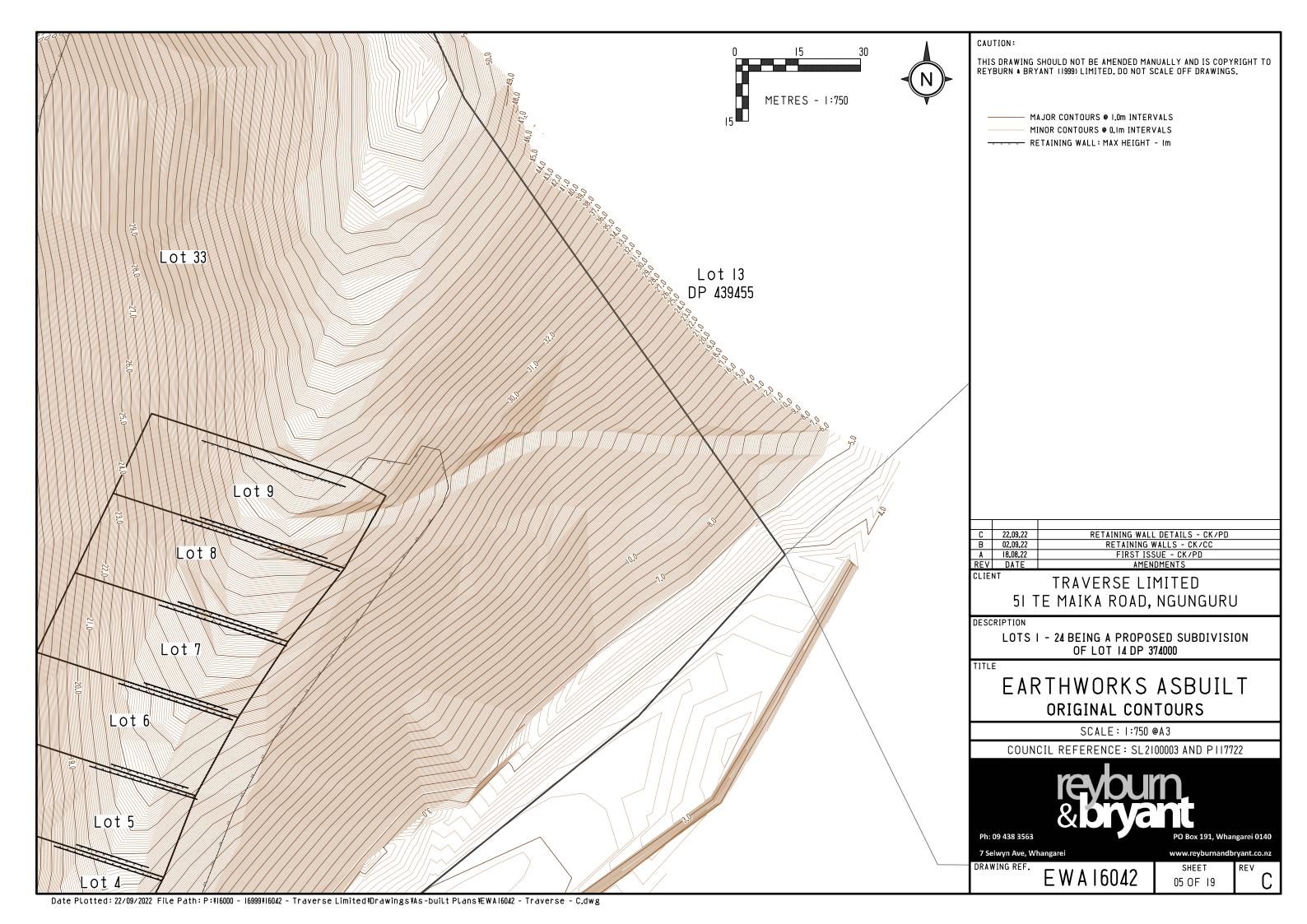
Job No: 20-0078

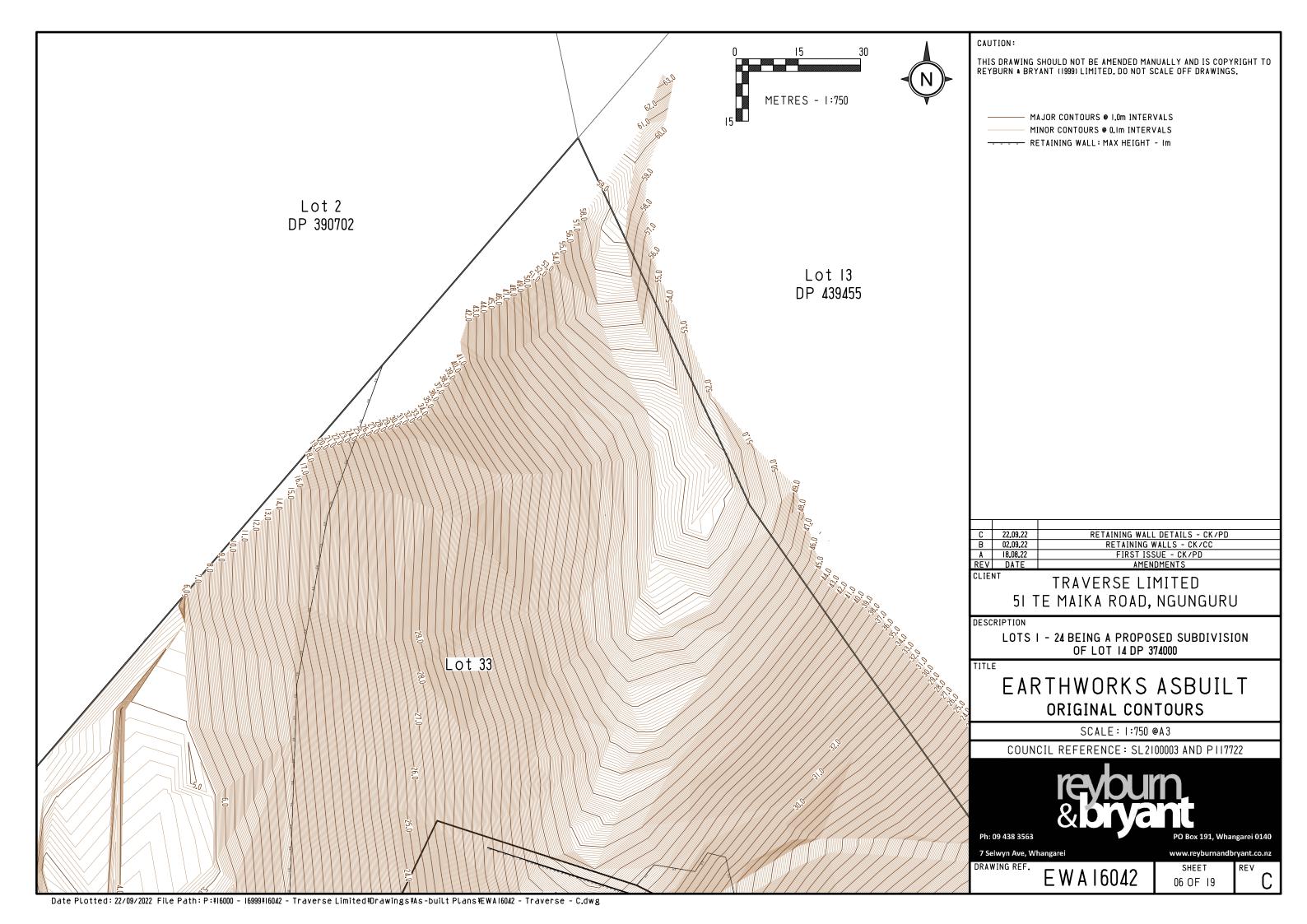


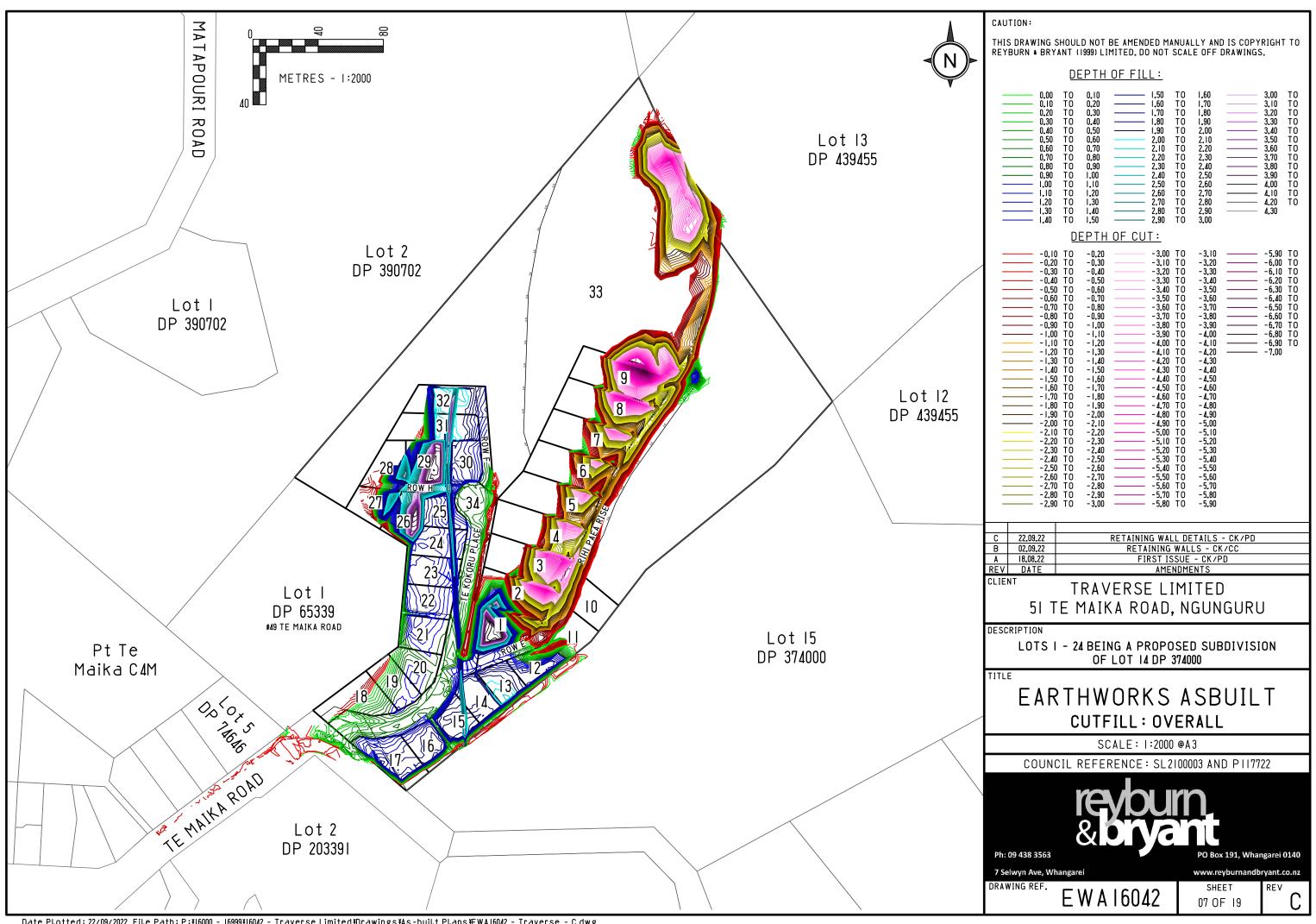


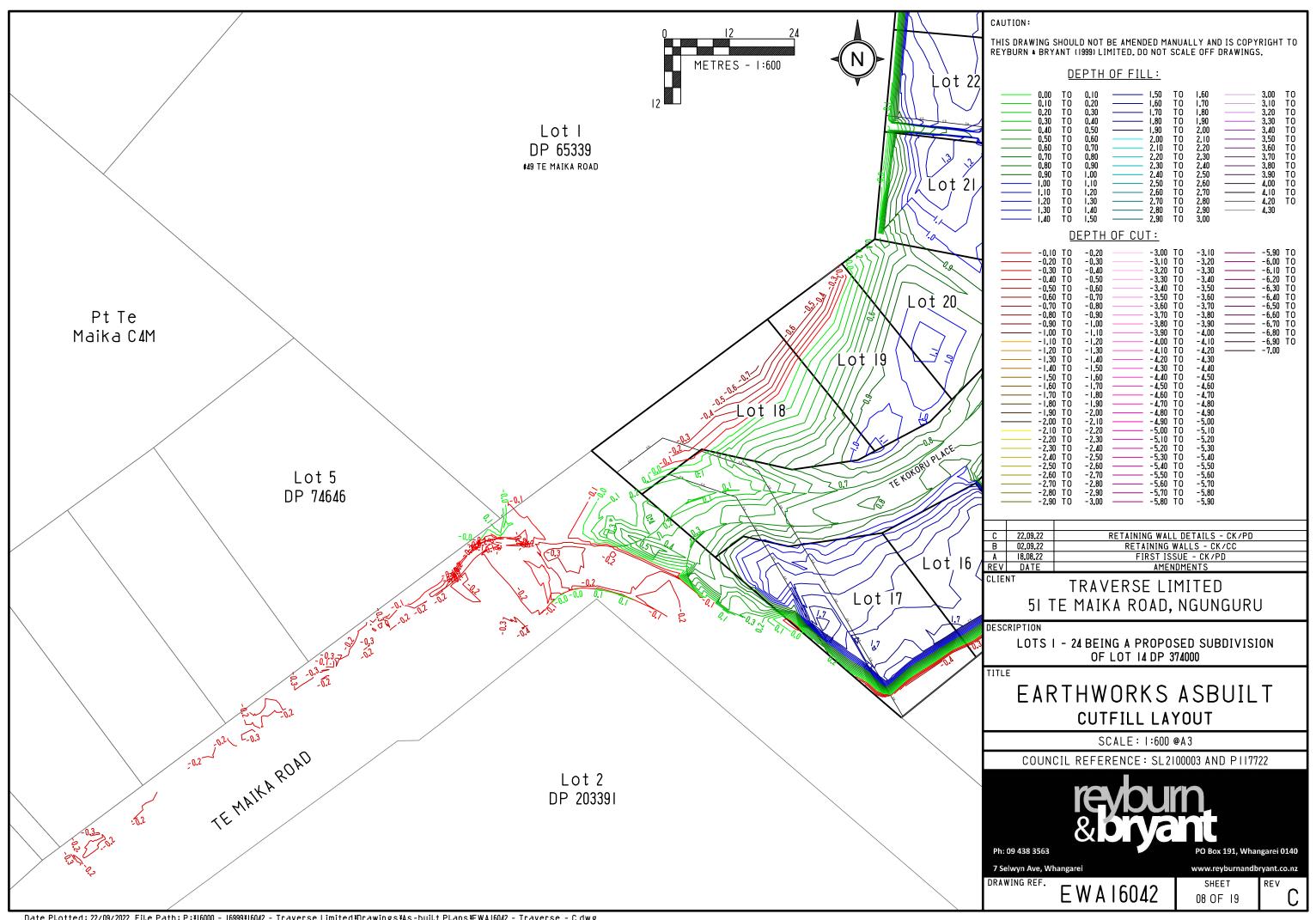


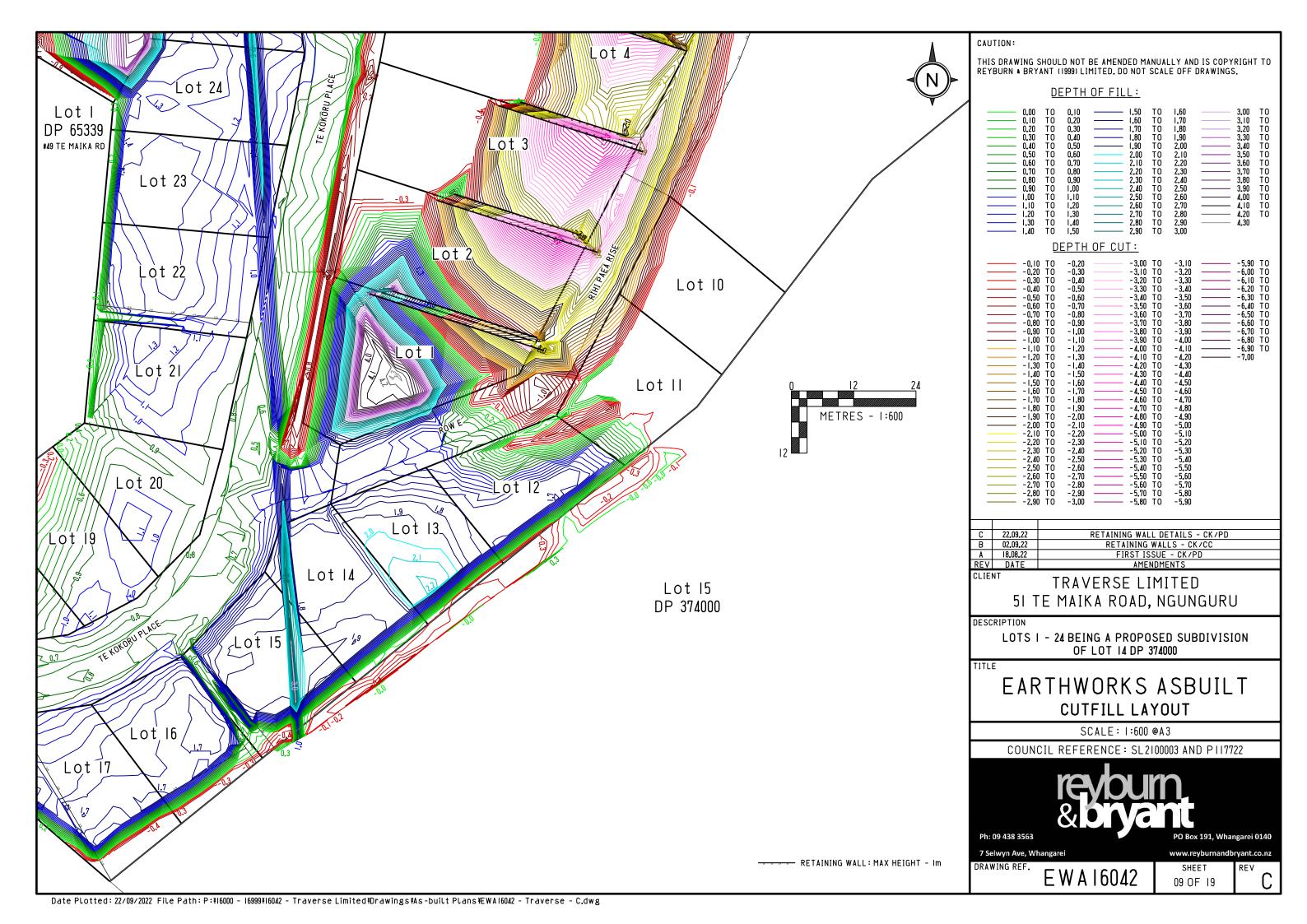


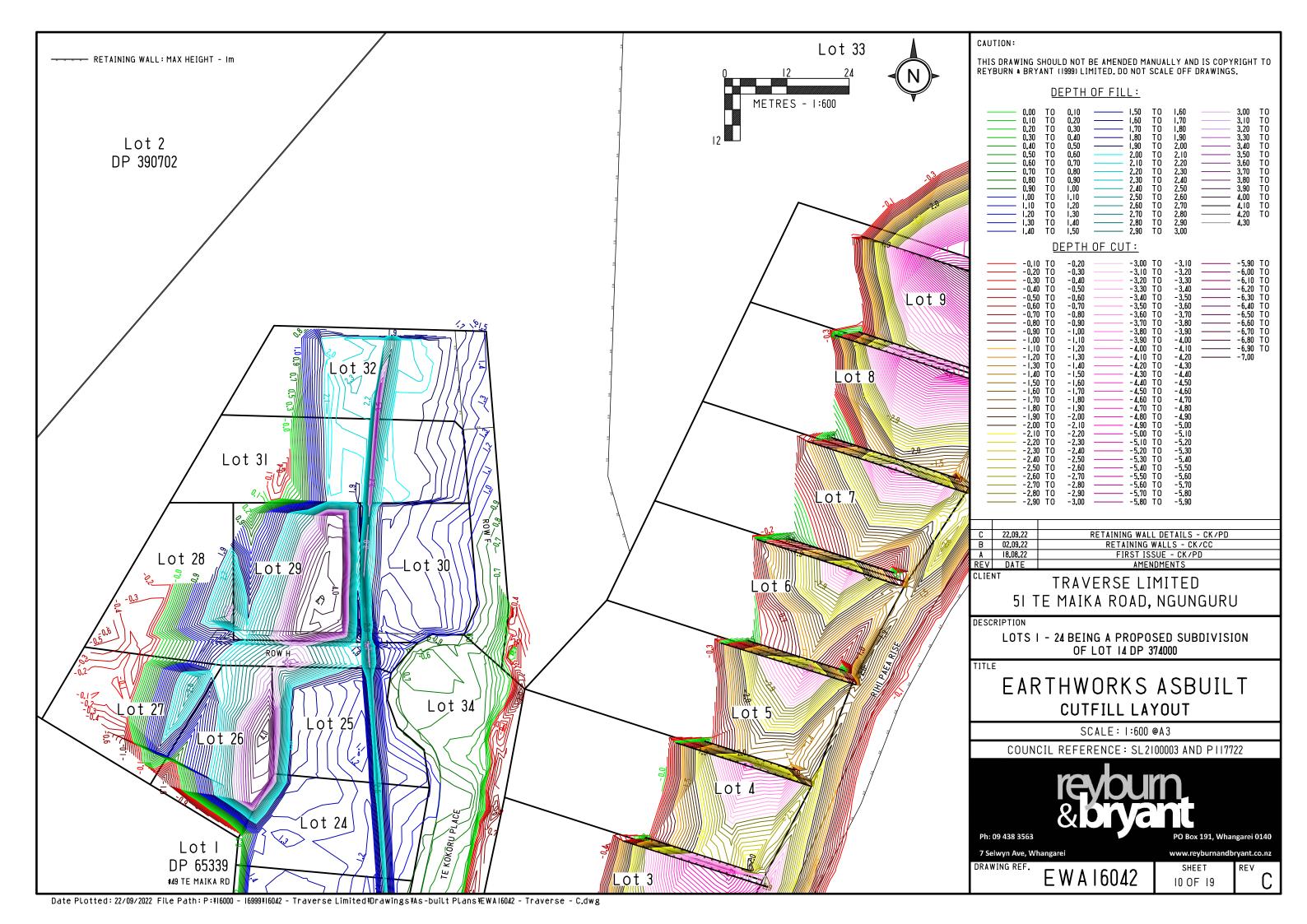


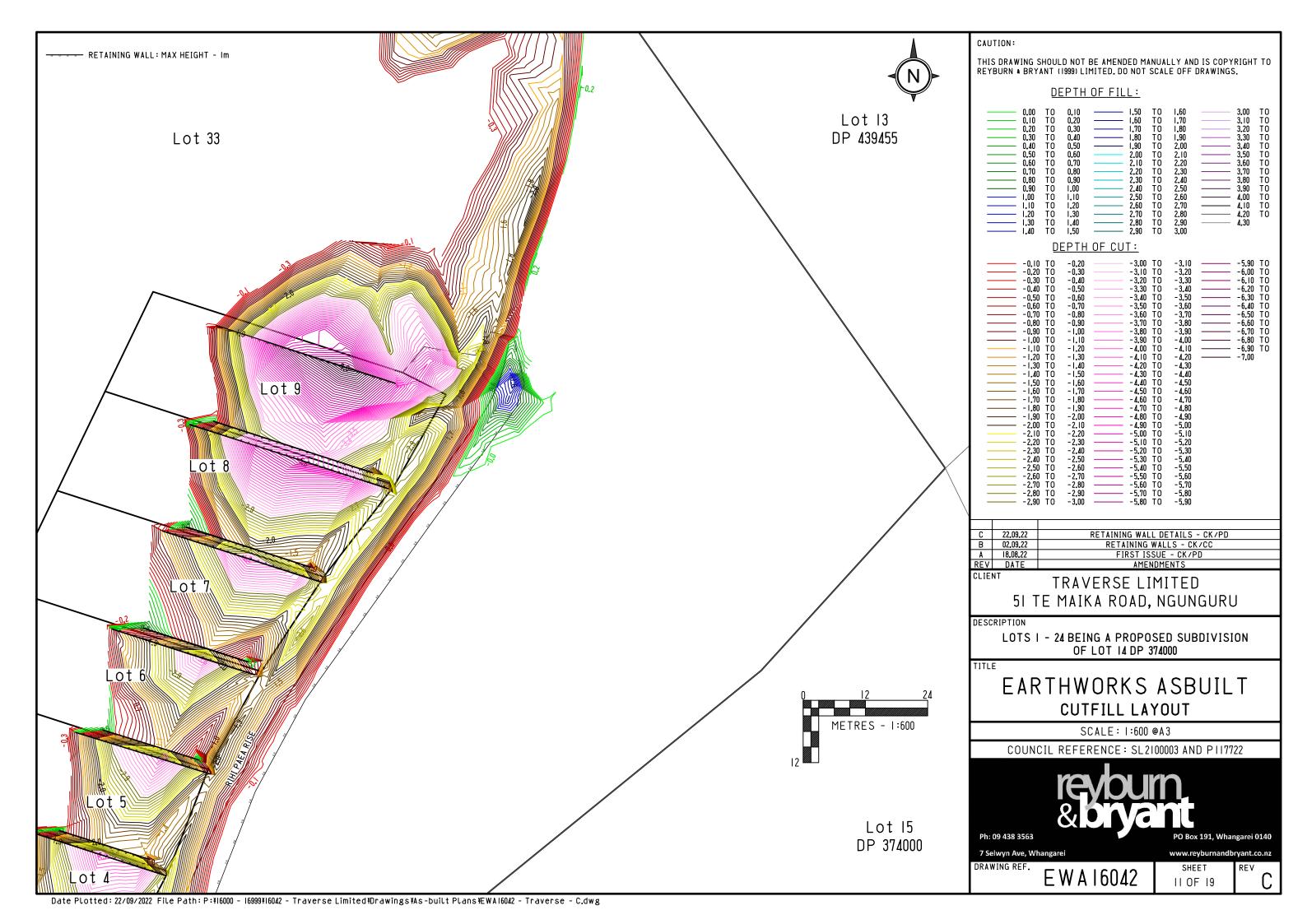


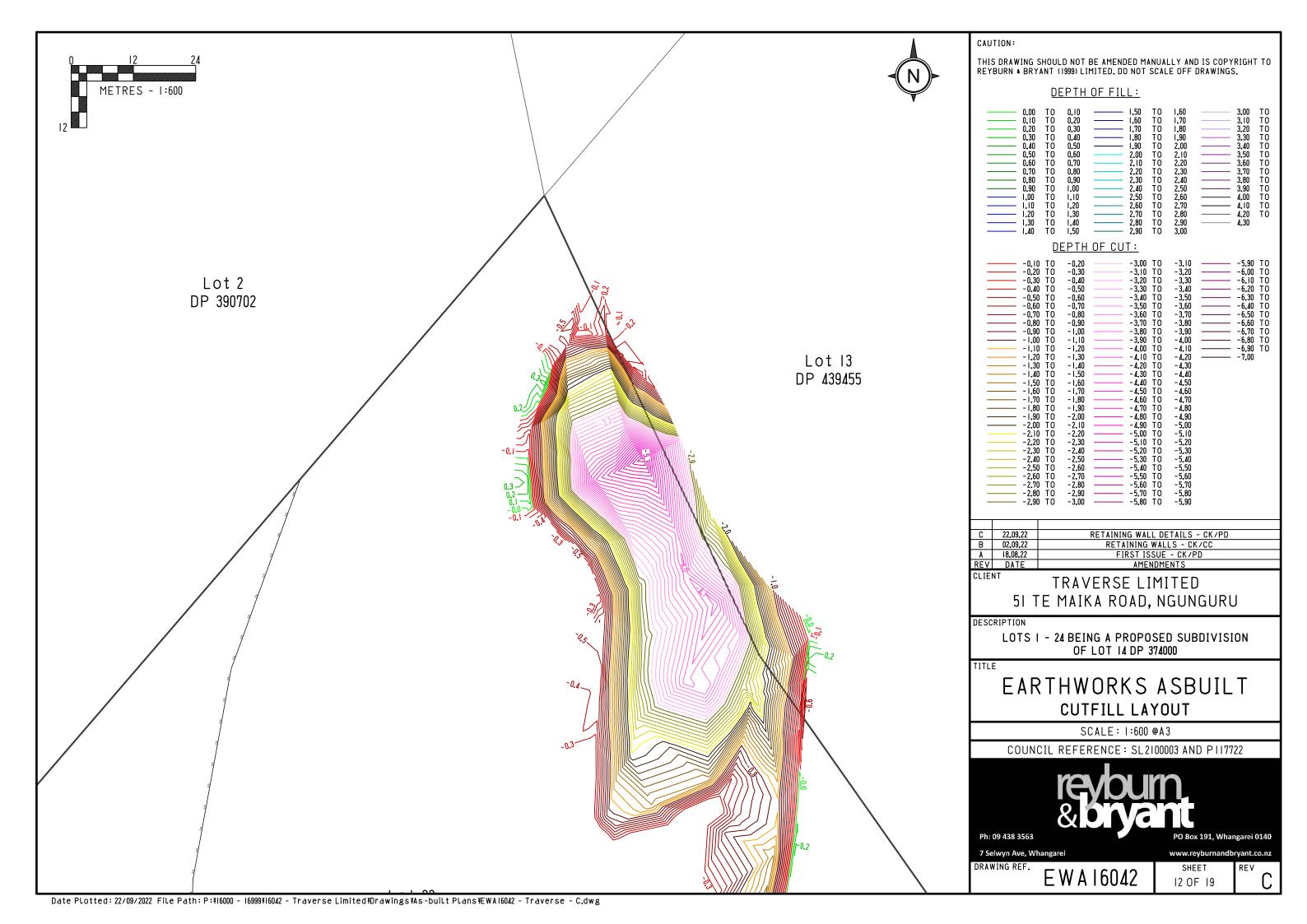


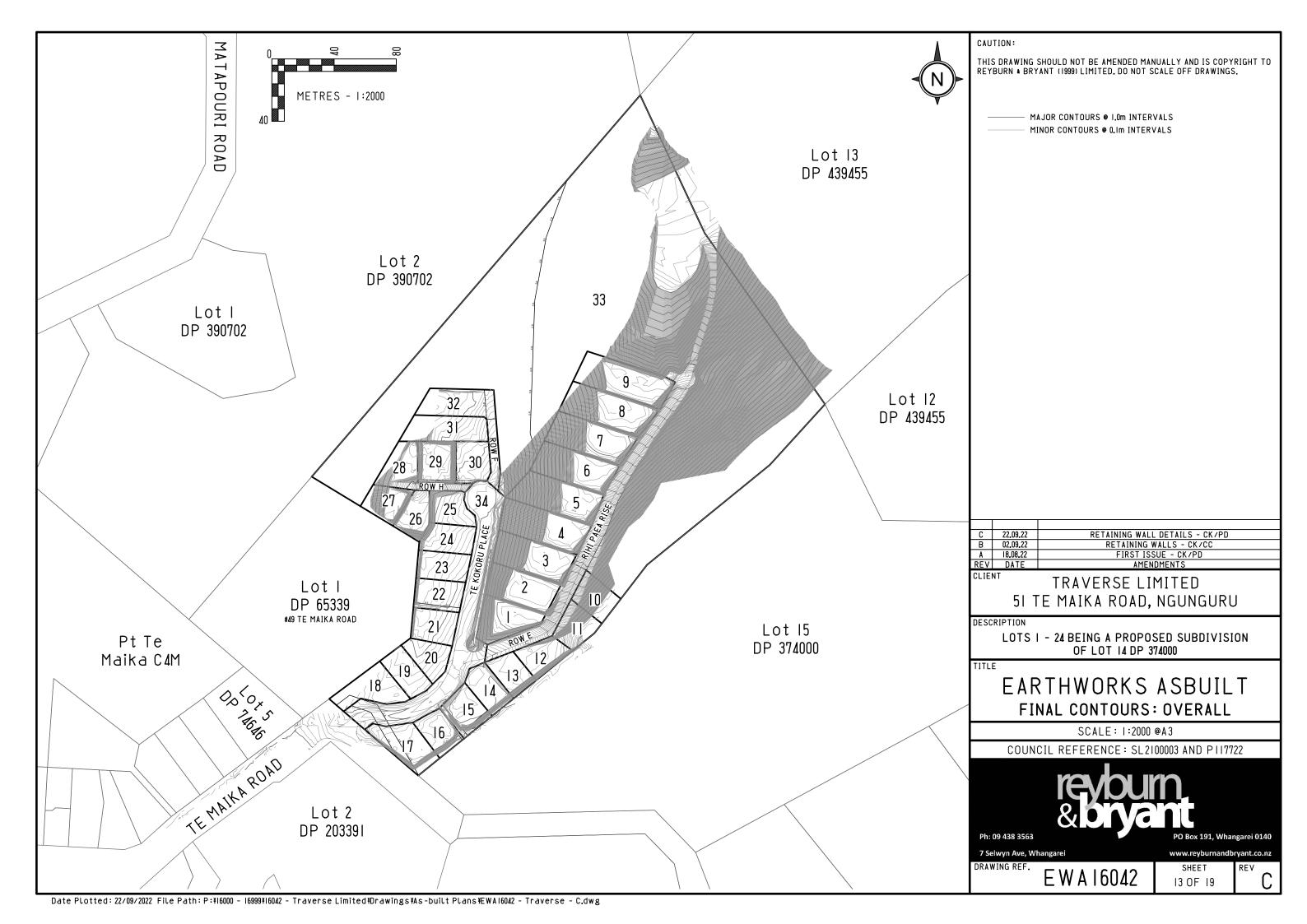


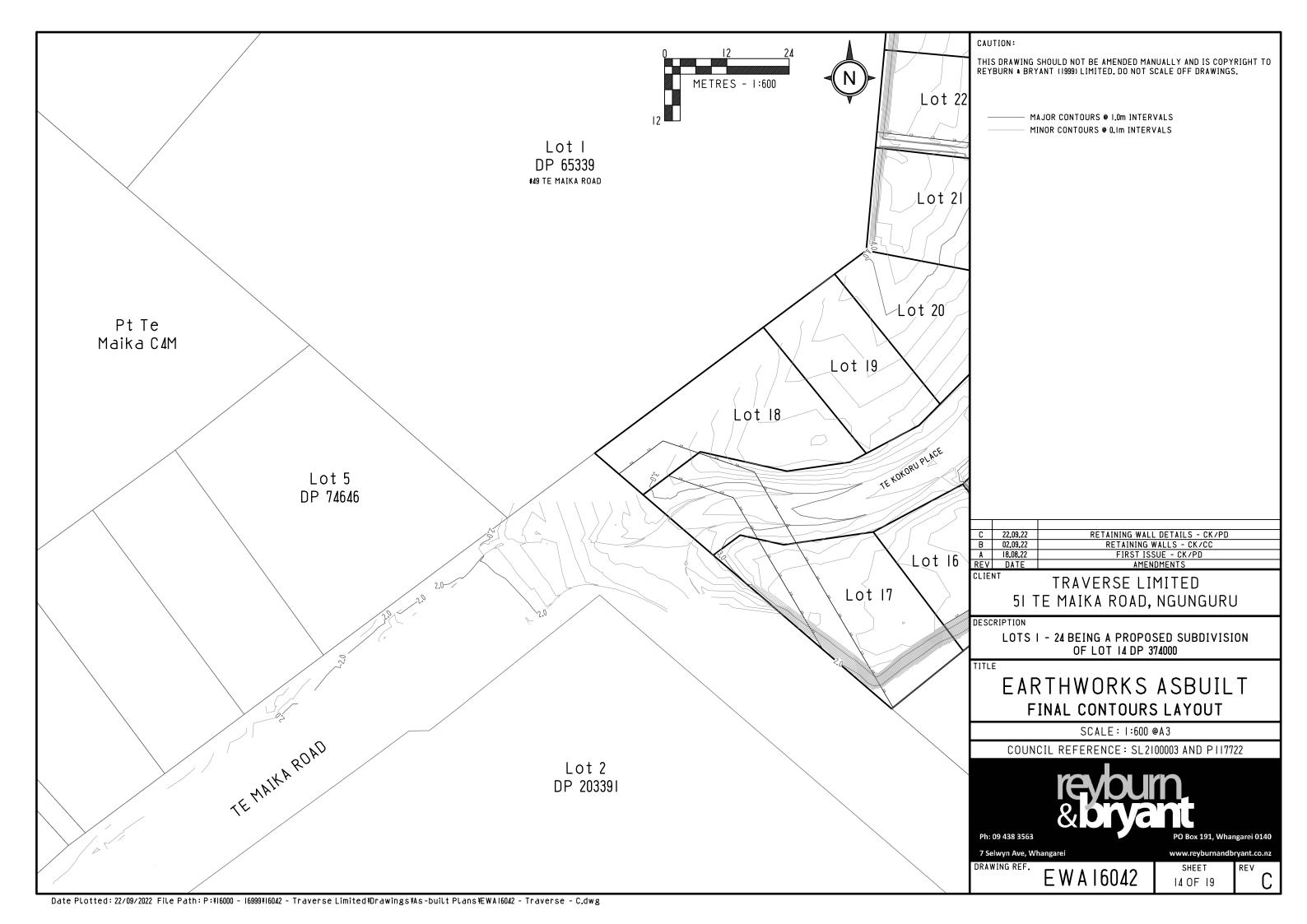


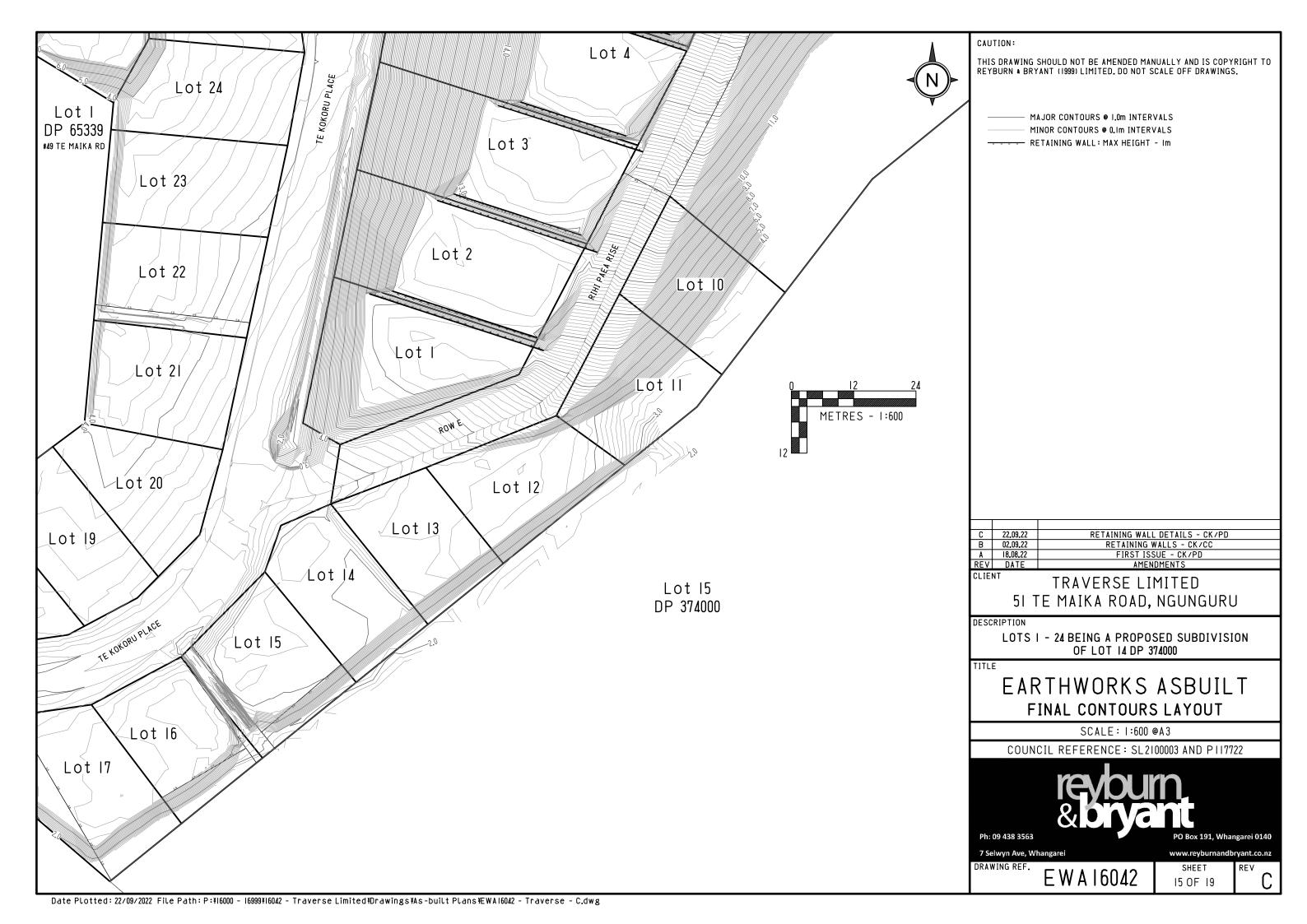


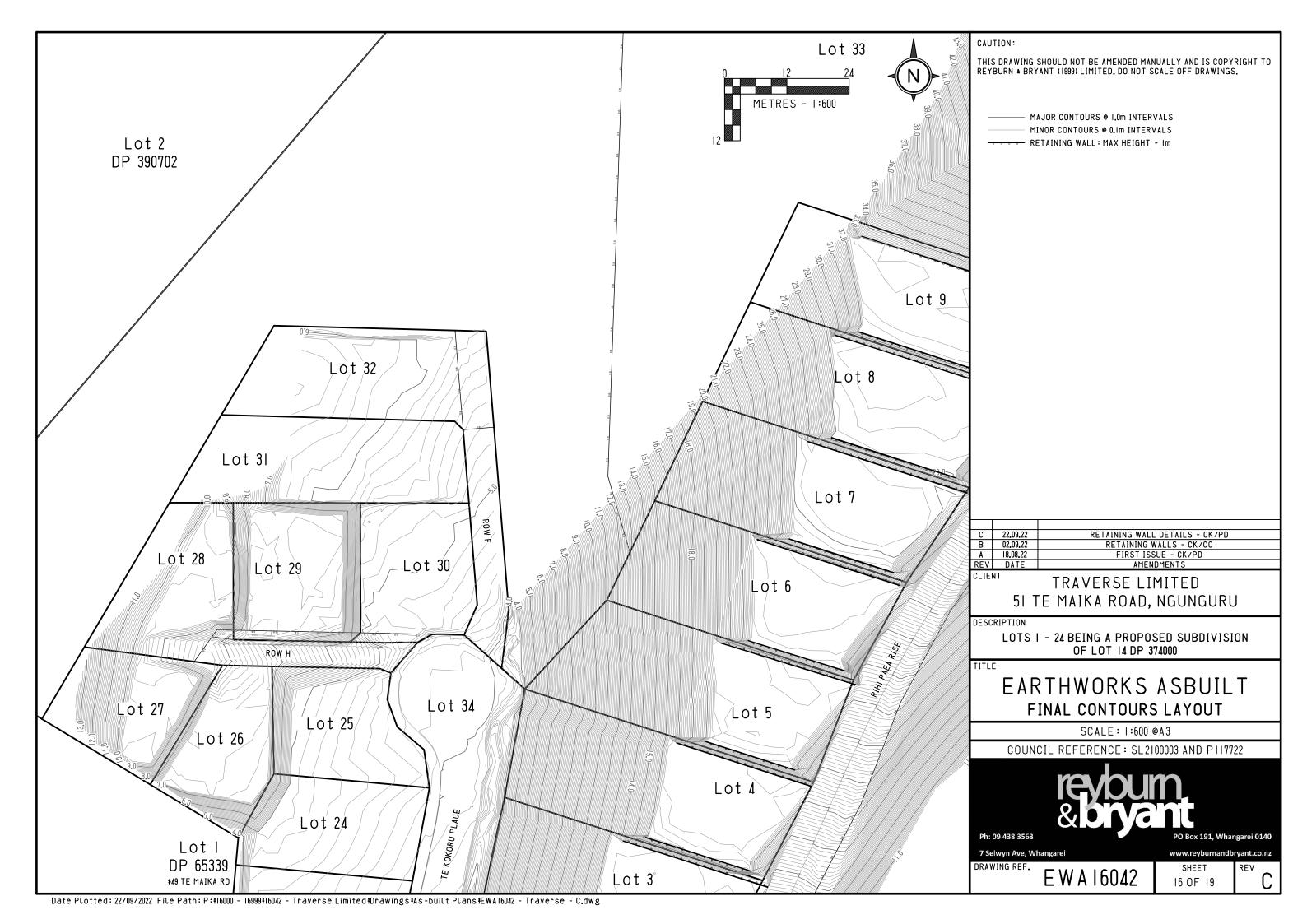


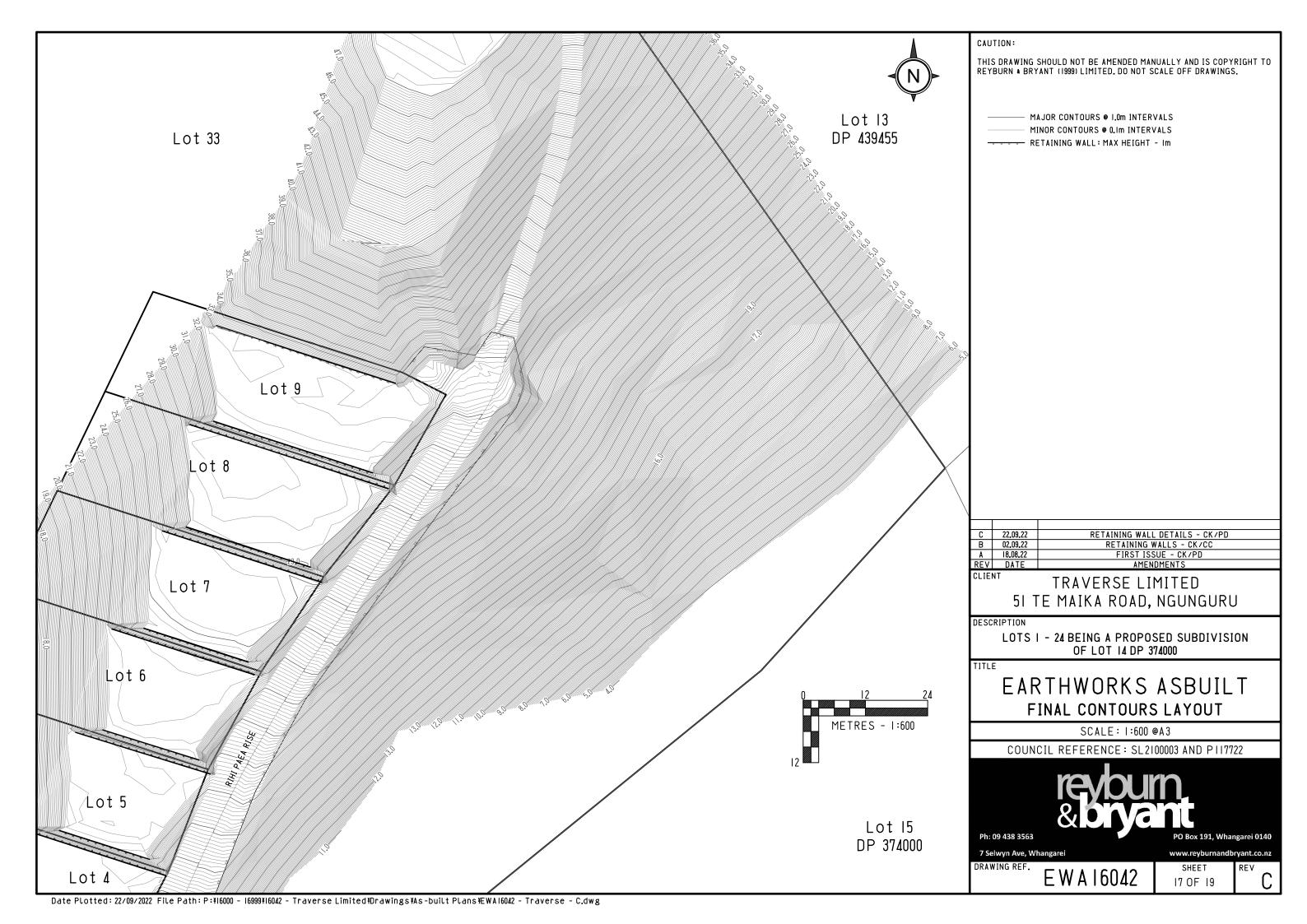


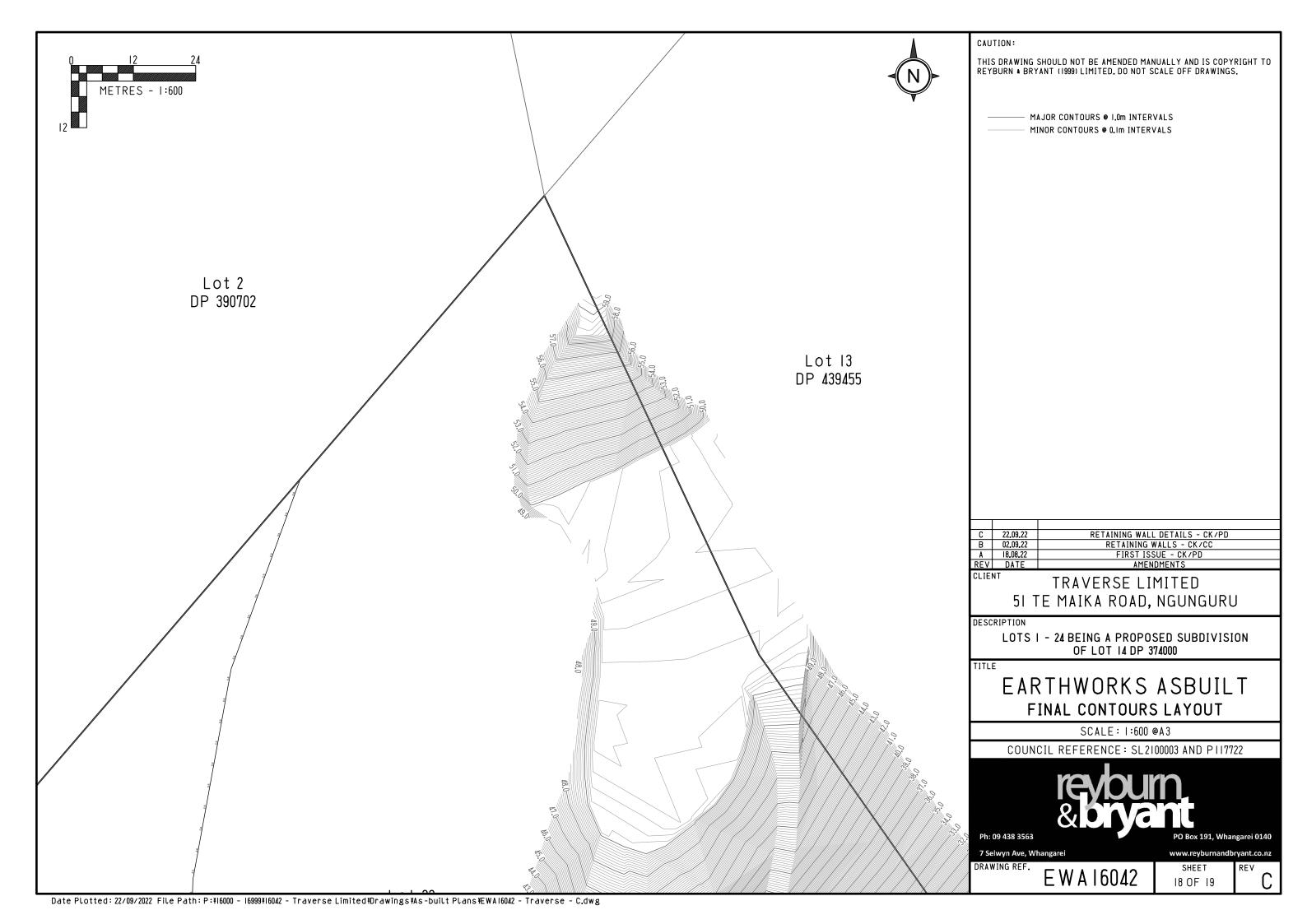


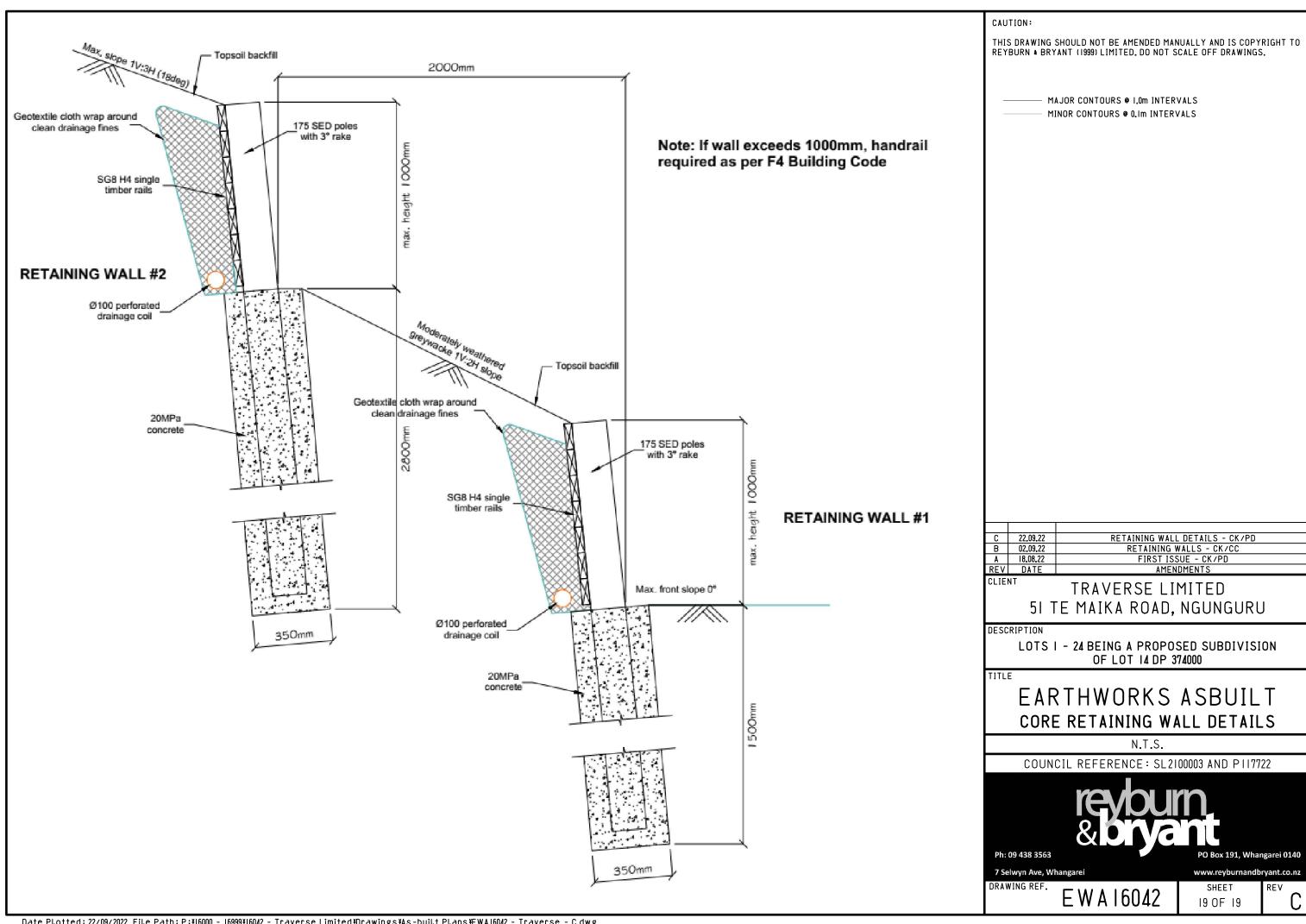






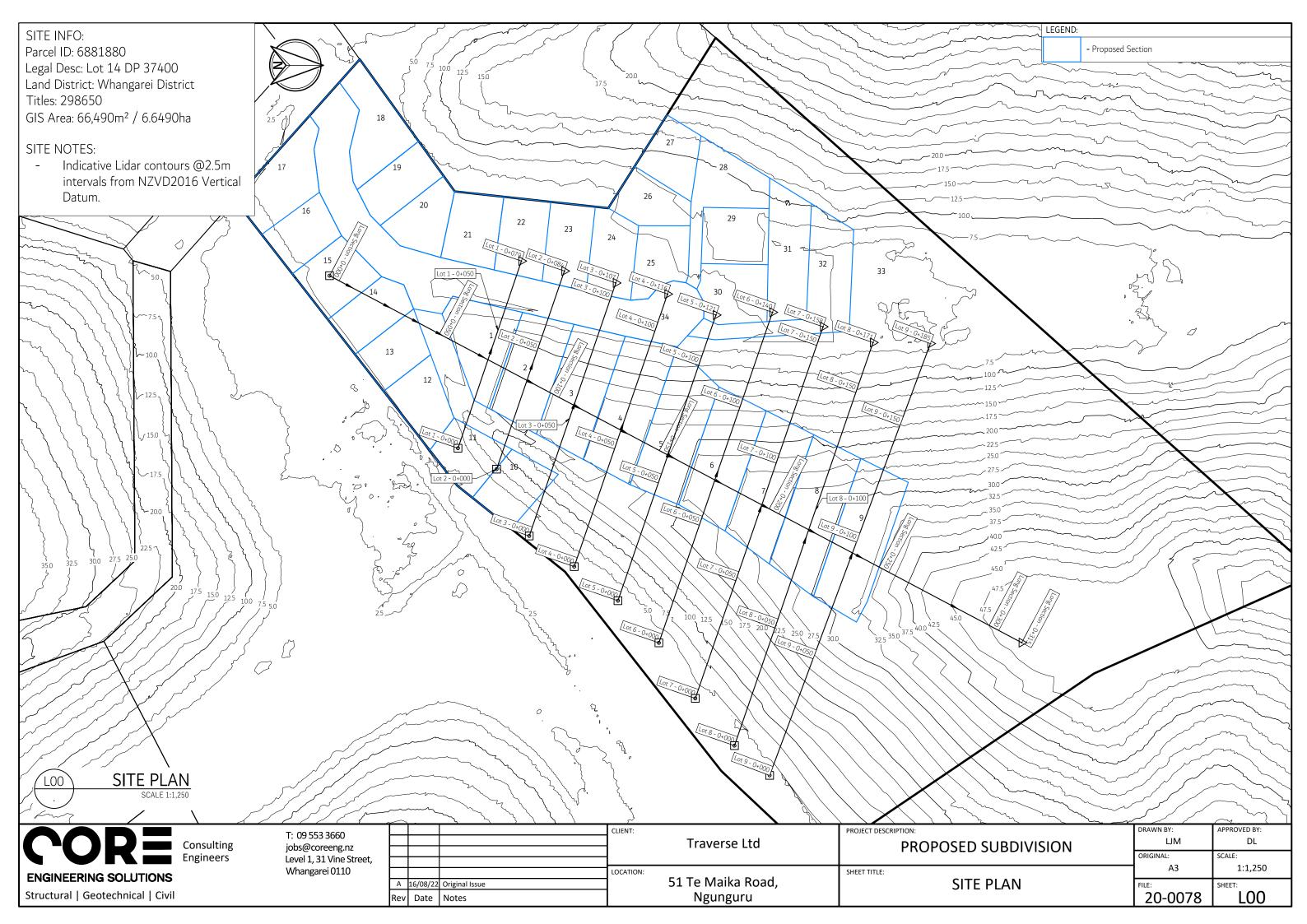


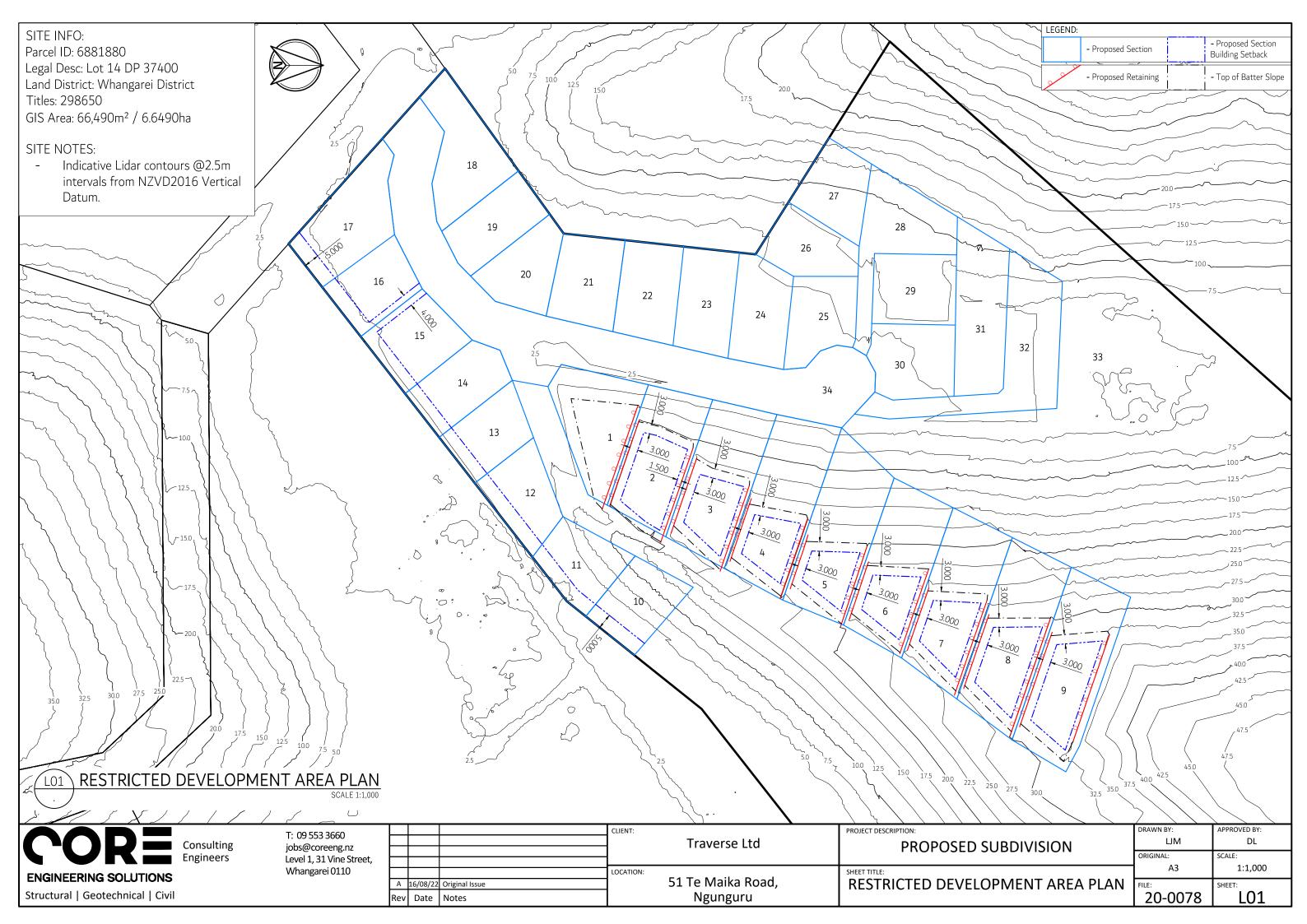


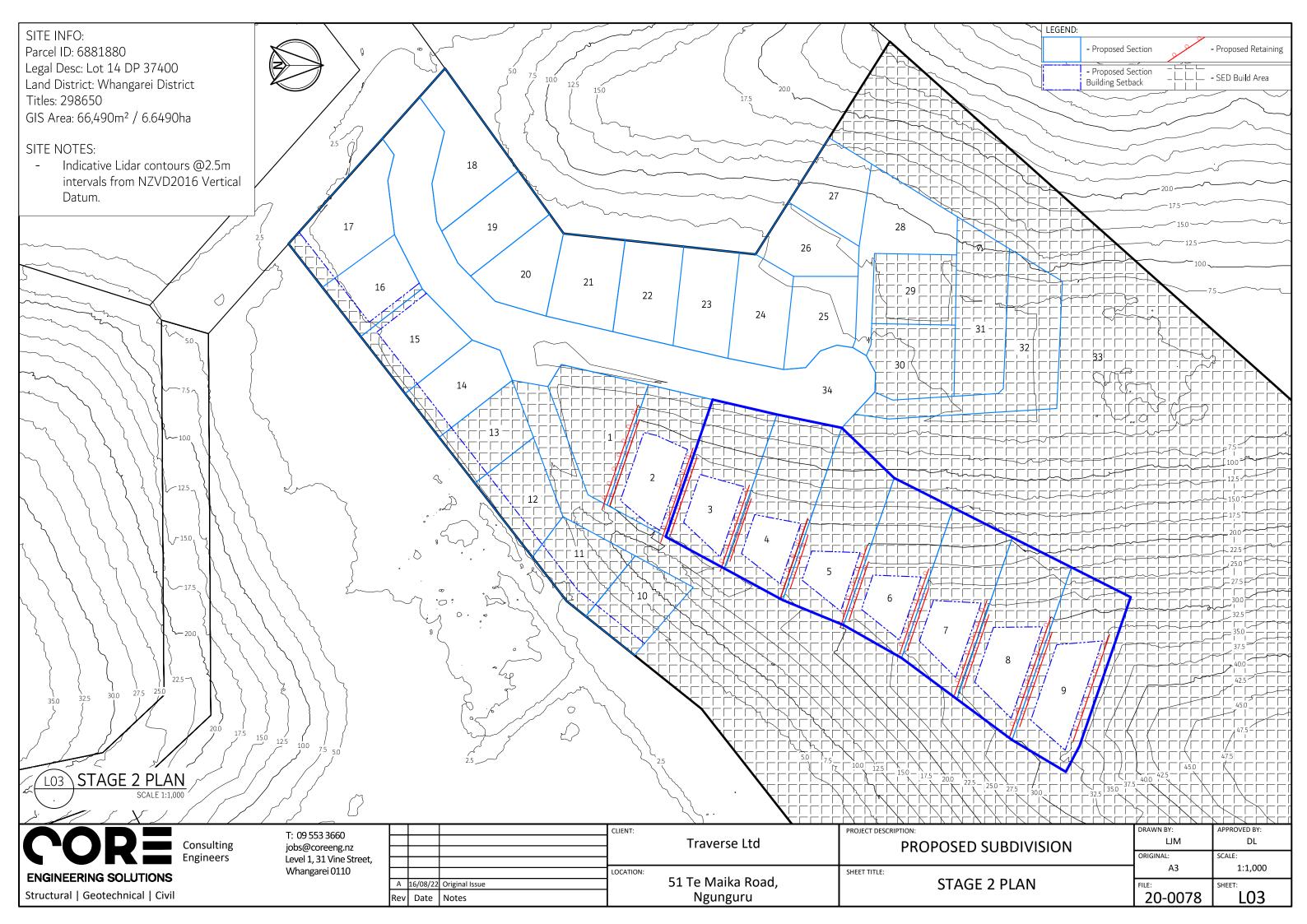


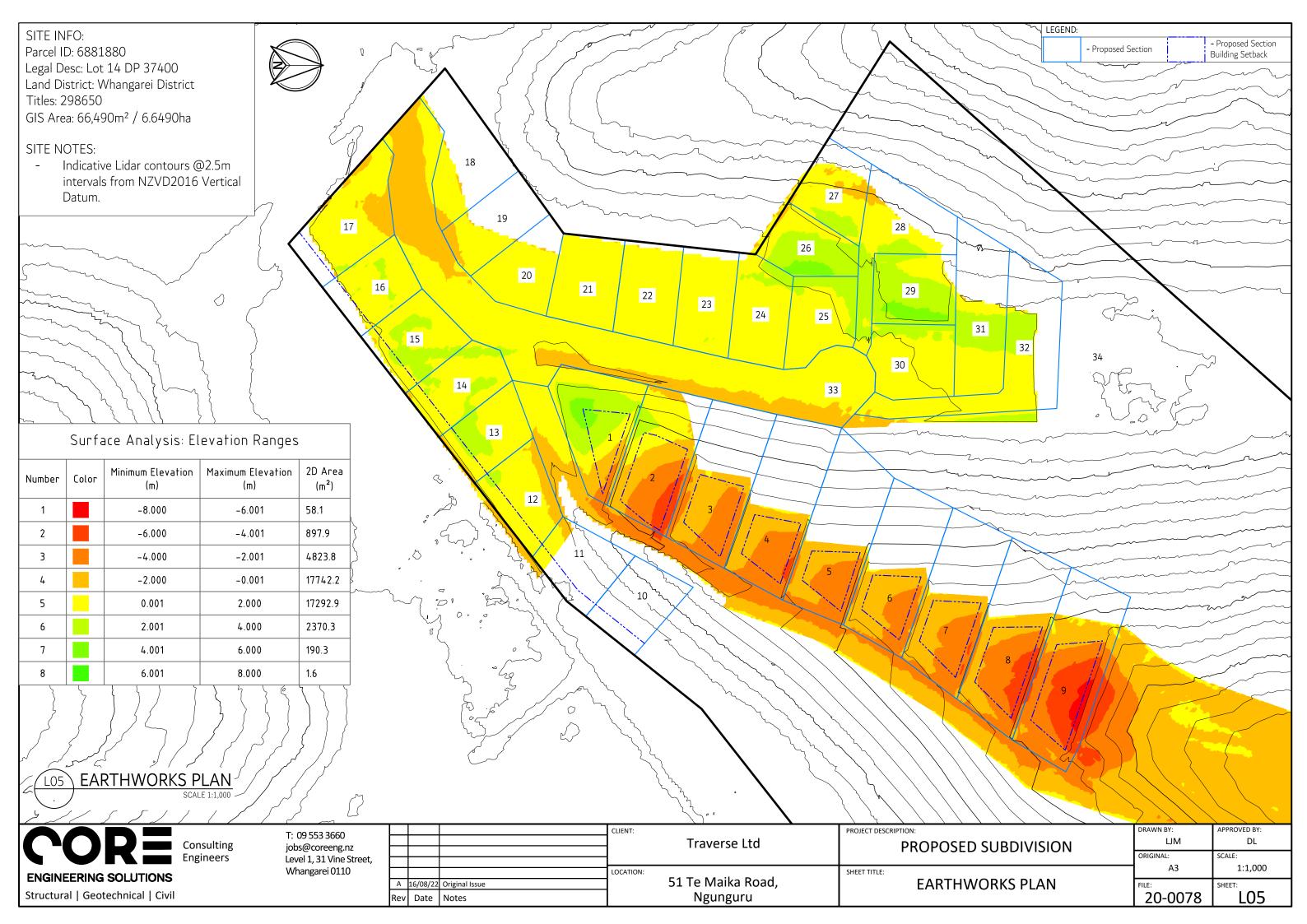


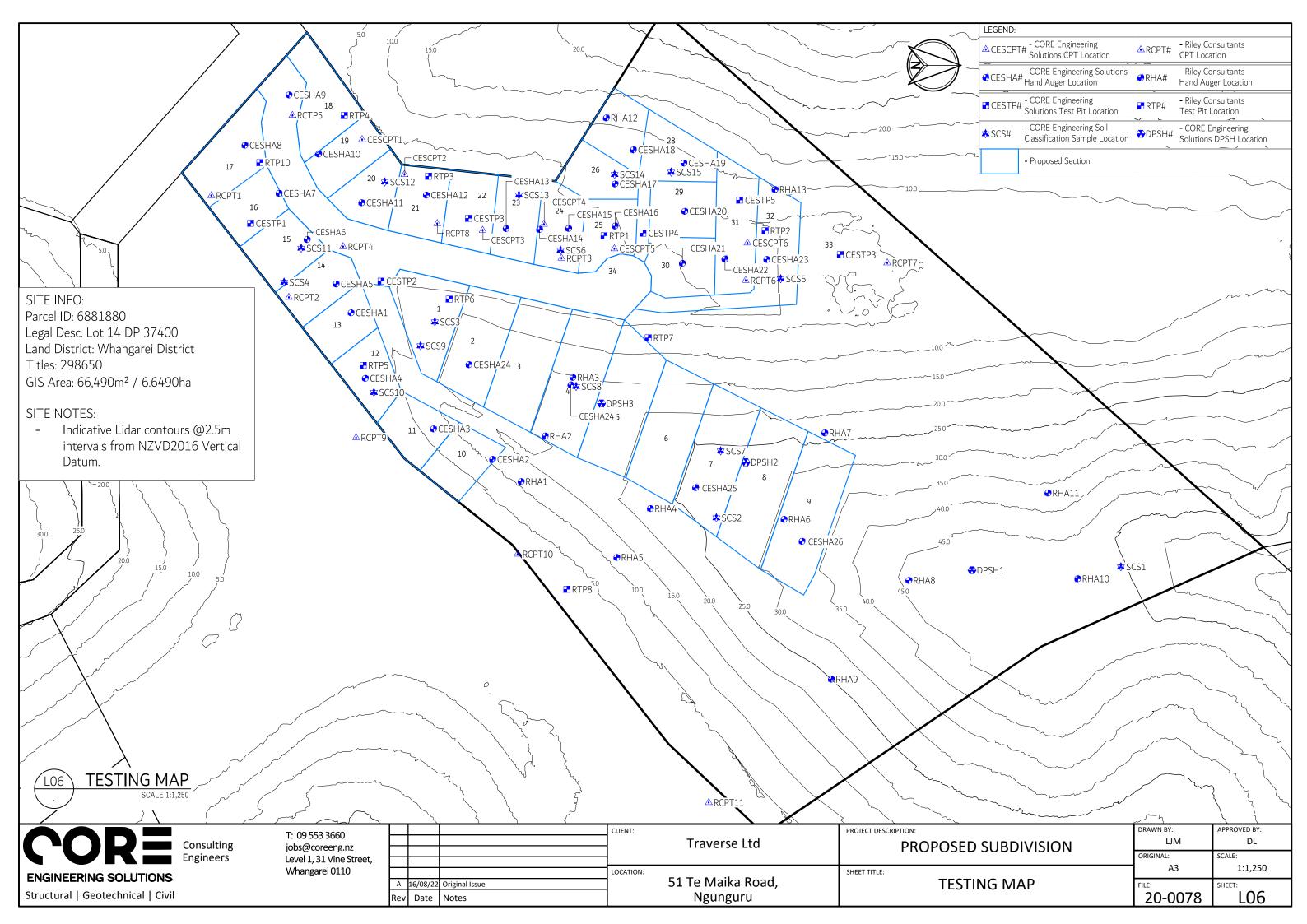
APPENDIX 4 - CORE ENGINEERING SOLUTIONS LTD DRAWINGS SET













APPENDIX 5 – TESTING RESULTS

CORE	INVESTIGATION LOG					HOLE NO.:				
ENGINEERING SOLUTIONS	INVE	511	GATIC	N LOC	7			CE	SHA	25
CLIENT: TRAVERSE LTD								JOB NO		
PROJECT: TE MAIKA RD, NGUNGURU - SUBDIVISION SITE LOCATION: TE MAIKA RD, NGUNGURU							START	DATE: 22/0	20-0078 9/2022	
CO-ORDINATES: 1737439mE, 6056587mN								DATE: 22/0		
		_	1 1					ED BY: RL		
MATERIAL DESCRIPTION	SAMPLES	DEРТН (m)			PENETRO		VANE S	HEAR STR (kPa)	ENGTH	ËR
(See Classification & Symbology sheet for details)	AMP	l E	LEGEND		(Blows / 0mm)			Vane: V03	,	WATER
TOPSOIL; light brown.	Š	<u> </u>		2 4 6	8 10 12	14 16 18	- 50	150	Values	
Moist; high plasticity.	_		× × × × × × × × × × × × × × × × × × ×							
Silty CLAY; orange. Moist; high plasticity.			×							
		0.2	× × × ×							
			×						221+	
		_	× × × ×							
		0.4	× ×						-	
			× × × ×							
			× ×							73
		0.6	× × × ×						166	intered
			× ×				2		35	Encor
		-	×							er Not
		0.8	× × × ×							Groundwater Not Encountered
			×						110	Grour
		_	× × ×				7 11 1	•		
		1.0	× × ×						32	
			××××							
		-	× ×							
		1.2	× × × ×				: :		158	
		T 1.2	× ×						76	
		_	× × ×							
EOH: 1.40m		1.4	× ×							
		_ '.4								
		_	4							
		1.6	7							
		_	4							
		1.8	7							
		_	4							
PHOTO(S)	·				ı	REMARKS				
			BH Lot 3	w	ATER		INIVES	TICATION	LTVDE	
					ATER			TIGATION	NIYPE	_
				▼ Standing	Water Level			and Auger		
				✓ In flow			Ш™	est Pit		

ORE INVESTIGATION LOG					HOLE NO.:			
ENGINEERING SOLUTIONS INVESTIGATION LOG								26
CLIENT: TRAVERSE LTD						JOB NO		
PROJECT: TE MAIKA RD, NGUNGURU - SUBDIVISION SITE LOCATION: TE MAIKA RD, NGUNGURU					START	DATE: 22/0	20-0078 9/2022	
CO-ORDINATES: 1737480mE, 6056637mN						DATE: 22/0	9/2022	
	ျှ	Ē				SHEAR STR	ENGTH	~
MATERIAL DESCRIPTION (See Classification & Symbology sheet for details)	SAMPLES	DEPTH (m)	LEGEND	SCALA PENETROMETER (Blows / 0mm)		(kPa) Vane: V03		WATER
(eee diabilities of a cympology sheet of actually	SAI	DEP	<u>"</u>	2 4 6 8 10 12 14 16	18 20 4		Values	8
TOPSOIL; light brown. \Moist; high plasticity.			× × ×					
Silty CLAY; orange tan brown. Moist; high plasticity; 0.9m white flecks.	_	0.2	× ×					
			× × ×		77		158	
		0.4	× ×		222		63	
		_	× ×				204	
		0.6	× × ×				221+	
		_	×					
		0.8	× × ×				145	
		_	× × ×		\square		39	
		1.0	× × ×					
		<u>ا</u>	× × × ×				174	
		1.2	× × ×		2		38	red
		1.4	× × × ×					counter
			× × × ×				161	Not Enc
		1.6	× × ×				47	water I
		L	× × × ×					Groundwater Not Encountered
EOH: 3.00m		1.8	×		7/3		205 60	O
		_	-				60	
		2.0	\dashv					
		_	1					
		2.2	-					
		١.,	7					
		2.4						
		2.6]					
		2.8	_					
		_	-					
PHOTO(S)		<u> </u>		REMARI	:	<u> </u>		
FILO 10(3)		-	BH Lot 7	REWARI	13			
				WATER		STIGATIO	N TYPE	
				▼ Standing Water Level> Out flow		land Auger		
				In flow	⊺	est Pit		

CORE	15137E	0 T I	0 A T10	N 1 00		HOLE NO.	:	
ENGINEERING SOLUTIONS	INVE	511	GATIO	N LOG		CES	HA2	27
CLIENT: TRAVERSE LTD						JOB NO.:		
PROJECT: TE MAIKA RD, NGUNGURU - SUBDIVISION SITE LOCATION: TE MAIKA RD, NGUNGURU	N				START	DATE: 22/09/2	-0078	
CO-ORDINATES: 1737501mE, 6056680mN					END	DATE : 22/09/2		
	(0					ED BY: RL		
MATERIAL DESCRIPTION	E	ᄪ	LEGEND	SCALA PENETROMETER	VANES	SHEAR STREN (kPa)	IGTH	WATER
(See Classification & Symbology sheet for details)	SAMPLES	DEPTH (m)	FE	(Blows / 0mm) 2 4 6 8 10 12 14 16	18 6 5	Vane: V03	Values	×
TOPSOIL; light brown.		Ť	# TO # # #			T T 9		
Moist; high plasticity. Silty CLAY; orange and white with black flecks.	-1	_	× × ×					
Moist; high plasticity.			× × × × ×					
		0.2	×				193	
		H	× × ×					
		0.4	× ×		24		39	
			× × ×					
		-	× ×				205	
		0.6	×		221		205	
			× × × × ×				44	_
			× ×					ıntered
		0.8	× × × ×					Groundwater Not Encountered
			× × ×				158	ter No
			× × × ×		2		44	undwa
Silty CLAY; tan brown/orange.		1.0	× × × × × ×					Gro
Moist; high plasticity; 1.7 UTP.		L	× ×					
			× × × ×					
		1.2	× × × × ×				221+	
		-	× ×					
		1.4	×××				-	
			× ×					
		-	× × ×				221+	
		1.6	× ×				221+	
EOH: 1.70m			×				-	
		1.8	-					
		L						
PHOTO(S)	· ·			REMAR	KS	· · · · · · · · · · · · · · · · · · ·		
			BH Lot 9	WATER		STIGATION 1	TYPE	-
				▼ Standing Water Level Out flow In flow		est Pit		



Whangarei Laboratory

166 Bank Street, Whangarei M: 021 0263 7711 E: martin@geocivil.co.nz

TEST REPORT

Lab Job No: 8690-001

Your ref.: -

Date of Issue: 12/07/2022

Date of Re-Issue:

Page: 1 of 9

<u>Test Report No.</u> WRE8690-001-R001

PROJECT: Te Maika Road - Soil Classification Testing

CLIENT: Core Engineering Solutions

Level 1, 31 Vine Street

ATTENTION: Stuart Gemmell

TEST METHODS: Determination of the liquid & plastic limits, plasticity index and water content

NZS 4402:1986 Tests 2.1,2.2,2.3,2.4 Determination of the Linear Shrinkage

NZS 4402:1986 Test 2.6

SAMPLING METHOD: Sampled by client - Sampling not accredited

TEST RESULTS: As per attached sheets

A. Agnew D. Krissansen

Laboratory Technician Approved Signatory



All tests reported herein have been performed in accordance with the laboratory's scope of accreditation



DETERMINATION OF THE LIQUID & PLASTIC LIMITS, PLASTICITY INDEX & WATER CONTENT

NZS 4402:1986 Test 2.2,2.3,2.4

Lab Job No: 8690-001 Sample No.: WRE8690-001-S001

Client: Core Engineering Solutions Tested By: N.K Location: Te Maika Road **Date Tested:** 1/07/2022 Checked By: Sample 1 A.A

Date Received: 17/06/2022 Date Checked: 8/07/2022 WRE8690-001-R001 Report No: Page: 2 of 9

REF:

Sampling Method: Sampled by client - Sampling not accredited Sampled By: Client

Date Sampled: 15/06/2022

Test Details:

Test performed on: Fraction passing 425 µm sieve

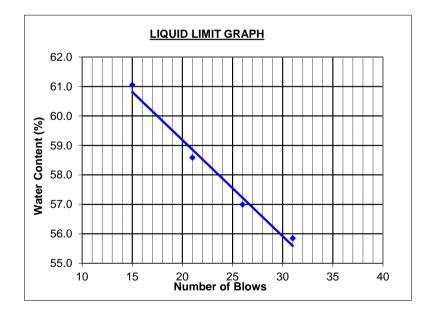
Natural state Sample history:

Description of Sample: Clayey SILT, minor fine sands to 2mm, light red mottled brown and grey, moist

	Liquid Limit						
No. of blows	15	21	26	31			
Water content (%)	61.1	58.6	57.0	55.8			

Plastic Limit					
34.7	34.5				

NWC	41.2
Liquid Limit	58
Plastic Limit	35
Plasticity Index	23



WRE8690-001-S001

N.K 1/07/2022

A.A

3 of 9

8/07/2022



DETERMINATION OF THE LINEAR SHRINKAGE

NZS 4402:1986 Test 2.6

Sample No:

Tested By:

Date: Checked By:

Date:

Page:

Lab Job No: 8690-001

Client: Core Engineering Solutions

Location: Te Maika Road

Sample 1

Date Received: 17/06/2022 Report No: WRE8690-001-R001

REF:

Test performed on: Fraction passing 425mm sieve

History: Natural state

Description of Sample: Clayey SILT, minor fine sands to 2mm, light red mottled brown and grey,

Linear shrinkage	13
------------------	----



Whangarei Laboratory

166 Bank Street, Whangarei M: 021 0263 7711 E: martin@geocivil.co.nz

TEST REPORT

Lab Job No: 8690-001

Your ref.:

Date of Issue: 27/09/2022

Date of Re-Issue:

Page: 1 of 5

<u>Test Report No.</u> WRE8690-001-R002

PROJECT: Te Maika Road - Soil Classification Testing

CLIENT: Core Engineering Solutions

Level 1, 31 Vine Street

ATTENTION: Stuart Gemmell

TEST METHODS: Determination of the liquid & plastic limits, plasticity index and water content

NZS 4402:1986 Tests 2.1,2.2,2.3,2.4 Determination of the Linear Shrinkage

NZS 4402:1986 Test 2.6

SAMPLING METHOD: Sampled by client - Sampling not accredited

TEST RESULTS: As per attached sheets

N. Krissansen D. Krissansen

Laboratory Technician Approved Signatory



All tests reported herein have been performed in accordance with the laboratory's scope of accreditation

DIE



DETERMINATION OF THE LIQUID & PLASTIC LIMITS, PLASTICITY INDEX & WATER CONTENT

NZS 4402:1986 Test 2.2,2.3,2.4

Lab Job No: 8690-001 Sample No.: WRE8690-001-S007

Client: Core Engineering Solutions Tested By: A.A/ N.K Location: Te Maika Road **Date Tested:** 22/09/2022

Checked By: N.K. Lot 7 Stage 2

6/09/2022 Date Checked: 27/09/2022 Date Received: Report No: WRE8690-001-R002 Page: 2 of 5

REF:

Sampling Method: Sampled by client - Sampling not accredited Sampled By: Client

Date Sampled: Unknown

Test Details:

Test performed on: Fraction passing 425 µm sieve

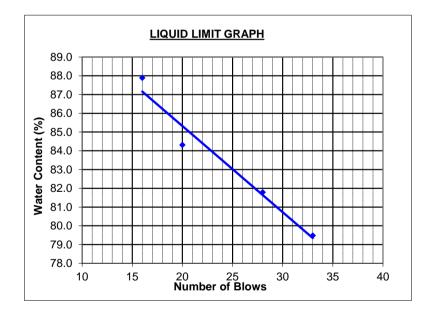
Sample history: As received

Description of Sample: Clayey SILT, minor fine sands, light red mottled orange, yellow and grey, moist

	Liquid Limit							
No. of blows	16	20	28	33				
Water content (%)	87.9	84.3	81.8	79.5				

Plastic Limit					
38.9	38.6				

NWC	38.9
Liquid Limit	83
Plastic Limit	39
Plasticity Index	44



WRE8690-001-S007

A.A 22/09/2022

N.K.

3 of 5

27/09/2022



DETERMINATION OF THE LINEAR SHRINKAGE

NZS 4402:1986 Test 2.6

Sample No:

Tested By:

Checked By:

Date:

Date:

Page:

Lab Job No: 8690-001

Client: Core Engineering Solutions

Location: Te Maika Road Lot 7 Stage 2

 Date Received:
 6/09/2022

 Report No:
 WRE8690-001-R002

REF: -

Test performed on: Fraction passing 425mm sieve

History: As received

Description of Sample: Clayey SILT, minor fine sands, light red mottled orange, yellow and grey, moist



DETERMINATION OF THE LIQUID & PLASTIC LIMITS, PLASTICITY INDEX & WATER CONTENT

NZS 4402:1986 Test 2.2,2.3,2.4

Lab Job No: 8690-001 Sample No.: WRE8690-001-S008

Client: Core Engineering Solutions Tested By: A.A/N.K Location: Te Maika Road **Date Tested:** 22/09/2022

Checked By: N.K. Lot 4, Stage 2

Date Checked: 27/09/2022 Date Received: 6/09/2022 Report No: WRE8690-001-R002 Page: 4 of 5

REF:

Sampling Method: Sampled by client - Sampling not accredited Sampled By: Client

Date Sampled: Unknown

Test Details:

Test performed on: Fraction passing 425 µm sieve

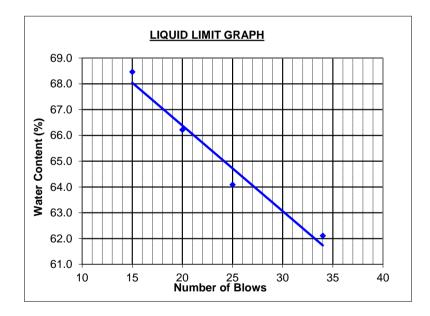
Sample history: As received

Description of Sample: Clayey SILT, traces of fine sands and rootlets, light red brown with black veins, moist

	Liquid Limit							
No. of blows	15	20	25	34				
Water content (%)	68.5	66.2	64.1	62.1				

Plastic Limit		
38.0	38.6	

NWC	46.5
Liquid Limit	65
Plastic Limit	38
Plasticity Index	27



D.Krissansen

WRE8690-001-S008

A.A

N.K.

5 of 5

22/09/2022

27/09/2022



DETERMINATION OF THE LINEAR SHRINKAGE

NZS 4402:1986 Test 2.6

Sample No:

Tested By:

Checked By:

Date:

Date:

Page:

Lab Job No: 8690-001

Client: Core Engineering Solutions

Location: Te Maika Road Lot 4, Stage 2

 Date Received:
 6/09/2022

 Report No:
 WRE8690-001-R002

REF: -

Test performed on: Fraction passing 425mm sieve

History: As received

Description of Sample: Clayey SILT, traces of fine sands and rootlets, light red brown with black

veins, moist

Linear shrinkage 11

Approved Signatory



APPENDIX 6 – GEOTECHNICAL PRODUCER STATEMENT PS4 FOR RETAINING WALLS







Building	Code	Clause(s	_{).} 1	

PRODUCER STATEMENT - PS4 - CONSTRUCTION REVIEW

ISSUED BY: Core Engineering Solution	s Ltd		
	(Construction Review I	Firm)	
TO: Traverse Ltd	(Owner/Developer)	
TO BE SUPPLIED TO: Whangarei Distr	rict Council (WDC) (Building Consent Auth		
IN RESPECT OF: Retaining Walls within	n Subdivision Works (Description of Building		
AT: 51 Te Maika Road,	, ,	,	
A1	(Address)		
Town/City: Ngunguru (Address)	LOT. ¹⁴	DP 374000	so
	have been engage	d by	
To provide CM1 CM2 CM3		ntegories) or observation a	as per agreement with
owner/developer.Traverse Ltd			
or other Construction Monitoring of co	onstruction of retaining walls (Extent of Engageme	nt)	services
in respect of clause(s) B1	of tl	ne Building Code for the build	ding work described in
documents relating to Building Consent I	No. Exempt works approved by	WDC	. and those relating to
Building Consent Amendment(s) Nos course of the works. We have eighted the	eee Building Censente and the	eenditions of attached to the	issued during the
Authorised instructions/variations(s) No. or by the attached Schedule nave bed			(copies attached)
On the basis of this review these and on behalf of the firm undertaking the All or Part only of the building we	nis Construction Review, I belie	ve on reasonable grounds	that
Building Consent and Building Consent A of the Building Code. I also believe on rethe necessary competency to do so.			
I, David Andrew Leslie (Name of Construction Review	am: ■	CPEng# Re	eg Arch#
I am a member of: Engineering New 2 The Construction Review Firm issuing this \$200,000*.	Zealand NZIA and hold the s statement holds a current police	following qualifications BEn by of Professional Indemnity I	g,DipCivil,MEMgt,CPEng nsurance no less than
The Construction Review Firm is a mem	ber of ACENZ:		
SIGNED BY David Andrew Leslie (Name of Cons	struction Review Professional)	(Signature)	
ON BEHALF OF Core Engineering Sol	utions Ltd (Construction Review F	 Firm)	Date 16/08/2022

Note: This statement shall only be relied upon by the Building Consent Authority named above. Liability under this statement accrues to the Design Firm only. The total maximum amount of damages payable arising from this statement and all other statements provided to the Building Consent Authority in relation to this building work, whether in contract, tort or otherwise (including negligence), is limited to the sum of \$200,000*.

This form is to accompany Forms 6 or 8 of the Building (Form) Regulations 2004 for the issue of a Code Compliance Certificate.

THIS FORM AND ITS CONDITIONS ARE COPYRIGHT TO ACENZ, ENGINEERING NEW ZEALAND AND NZIA

GUIDANCE ON USE OF PRODUCER STATEMENTS

Producer statements were first introduced with the Building Act 1991. The producer statements were developed by a combined task committee consisting of members of the New Zealand Institute of Architects, Institution of Professional engineers New Zealand (now Engineering New Zealand), Association of Consulting Engineers New Zealand in consultation with the Building Officials Institute of New Zealand. The original suit of producer statements has been revised at the date of this form as a result of enactment of the Building Act (2004) by these organisations to ensure standard use within the industry.

The producer statement system is intended to provide Building Consent Authorities (BCAs) with reasonable grounds for the issue of a Building Consent or a Code Compliance Certificate, without having to duplicate design or construction checking undertaken by others.

PS1 Design Intended for use by a suitably qualified independent design professional in circumstances where the BCA accepts a producer statement for establishing reasonable grounds to issue a Building Consent;

PS2 Design Review Intended for use by a suitably qualified independent design professional where the BCA accepts an independent design professional's review as the basis for establishing reasonable grounds to issue a Building Consent;

PS3 Construction Forms commonly used as a certificate of completion of building work are Schedule 6 of NZS 3910:2013 or Schedules E1/E2 of NZIA's SCC 2011²

PS4 Construction Review Intended for use by a suitably qualified independent design professional who undertakes construction monitoring of the building works where the BCA requests a producer statement prior to issuing a Code Compliance Certificate.

This must be accompanied by a statement of completion of building work (Schedule 6).

The following guidelines are provided by ACENZ, Engineering NZ and NZIA to interpret the Producer Statement.

Competence of Design Professional

This statement is made by a Design Firm that has undertaken a contract of services for the services named, and is signed by a person authorised by that firm to verify the processes within the firm and competence of its designers.

A competent design professional will have a professional qualification and proven current competence through registration on a national competence based register, either as a Chartered Professional Engineer (CPEng) or a Registered Architect.

Membership of a professional body, such as Engineering New Zealand (formerly IPENZ) or the New Zealand Institute of Architects (NZIA), provides additional assurance of the designer's standing within the profession. If the design firm is a member of the Association of Consulting Engineers New Zealand (ACENZ), this provides additional assurance about the standing of the firm.

Persons or firms meeting these criteria satisfy the term "suitably qualified independent design professional".

*Professional Indemnity Insurance

As part of membership requirements, ACENZ requires all member firms to hold Professional Indemnity Insurance to a minimum level.

The PI Insurance minimum stated on the front of this form reflects standard, small projects. If the parties deem this inappropriate for large projects the minimum may be up to \$500,000.

Professional Services during Construction Phase

There are several levels of service which a Design Firm may provide during the construction phase of a project (CM1-CM5 for Engineers³). The Building Consent Authority is encouraged to require that the service to be provided by the Design Firm is appropriate for the project concerned.

Requirement to provide Producer Statement PS4

Building Consent Authorities should ensure that the applicant is aware of any requirement for producer statements for the construction phase of building work at the time the building consent is issued as no design professional should be expected to provide a producer statement unless such a requirement forms part of the Design firm's engagement.

Attached Particulars

Attached particulars referred to in this producer statement refer to supplementary information appended to the producer statement.

Refer Also:

- Conditions of Contract for Building & Civil Engineering Construction NZS 3910: 2013
- NZIA Standard Conditions of Contract SCC 2011
- 3 Guideline on the Briefing & Engagement for Consulting Engineering Services (ACENZ/IPENZ 2004)
- 4 PN Guidelines on Producer Statements

www.acenz.org.nz www.engineeringnz.org www.nzia.co.nz







Te Kāhui Whaihanga New Zealand Institute of Architects

Producer Statements PS1, PS2, & PS4

ACEN7 engineer

October 2013



APPENDIX 7 - SLOPE STABILITY ANALYSIS RESULTS

A stability assessment was undertaken to ensure the long-term slope stability of the site as required under Section 2.2.3.3 of the WDC EES and in accordance with the WDC Land Development Stabilisation – Technical Design Requirements (WDC LDS). As outlined in WDC LDS, a minimum factor of safety for land stabilisation design is required for the following design conditions;

- Normal Long Term Groundwater Conditions = 1.5 FOS
- Extreme Groundwater Conditions = 1.3 FOS
- Seismic Conditions in 500 year Return Period Event = 1.1 FOS

CES Ltd adopted extremely conservative groundwater levels for "SLIDE" Slope Stability parameters. Steeper slopes are marked on the WDC GIS Hazards Maps as being at a high risk for instability. For this reason, CES Ltd adopted a worst-case scenario.

The Morgenstern-Price method has been adopted for the calculation of the factor of safety.

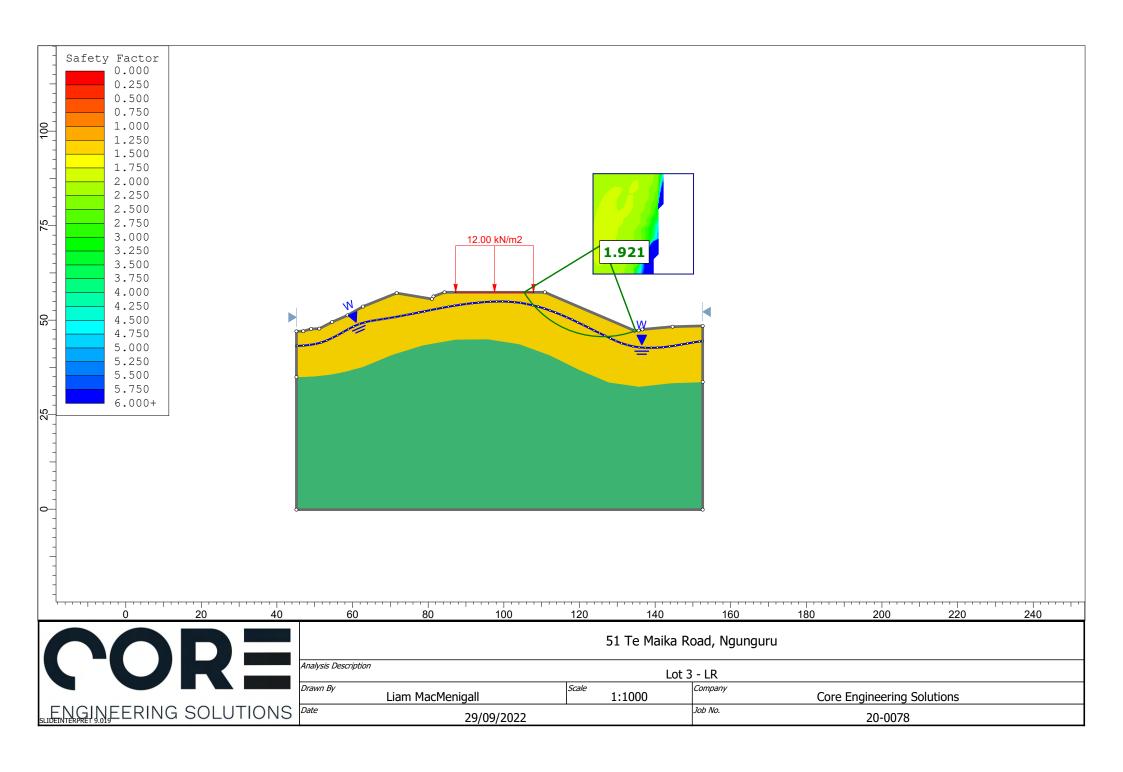
From the above information and assessment of the geomorphology, a section through the site has been developed using the above design conditions as scenarios using limited equilibrium software "Slide" version 6 by Rocscience. The underlying geomorphology is completely to highly weathered greywacke which gradually becomes weathered at depth. To determine the transition of the weathered material, DPSH testing was conducted at the top end of the flanks. Allowance for residential housing and roading surcharges are to be applied as part of the assessment of post-development conditions. Backanalysis of the site has been undertaken at the pre-development stage using both site observations and previous assessments within similar Waipapa Group ground conditions to validate the soil parameters used for the stability assessment. From this and the back-analysis, the following soil parameters were adopted for the stability assessment;

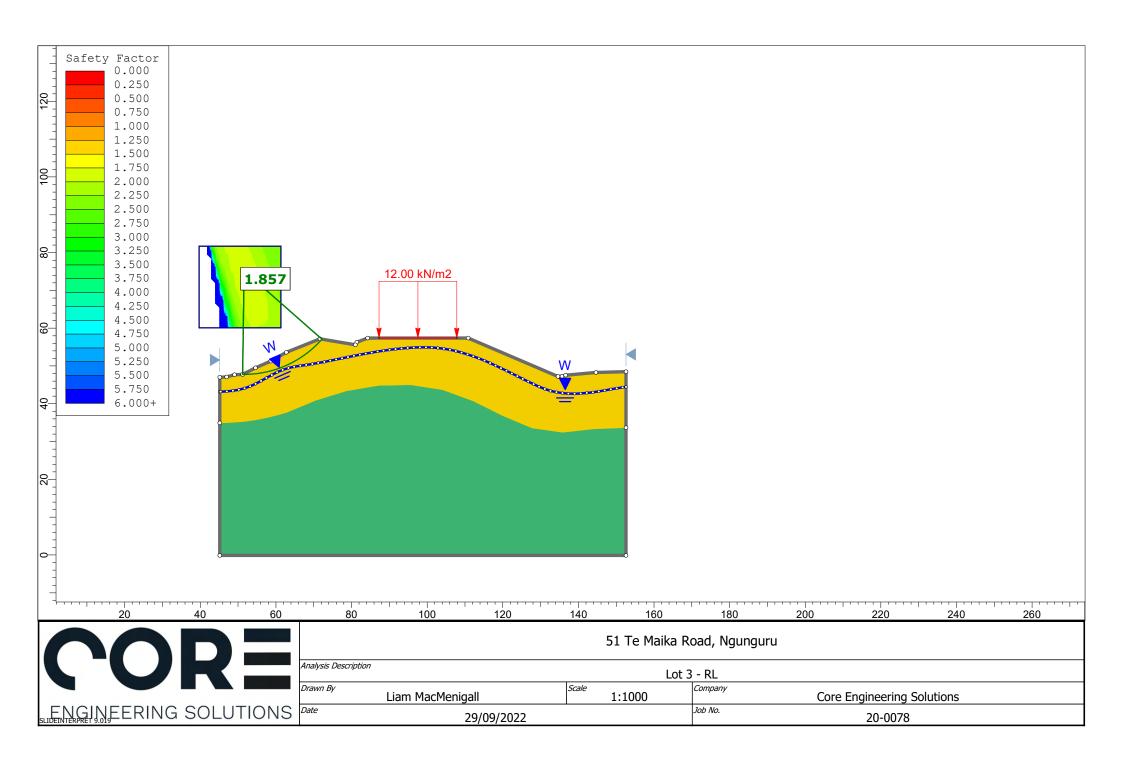
Soil Unit	Soil Unit Density Weight (kN/m³)	Angle of Internal Friction (¢')	Cohesion (kPa)
Completely Weathered GW	18	32	5
Highly Weathered GW	18	34	10

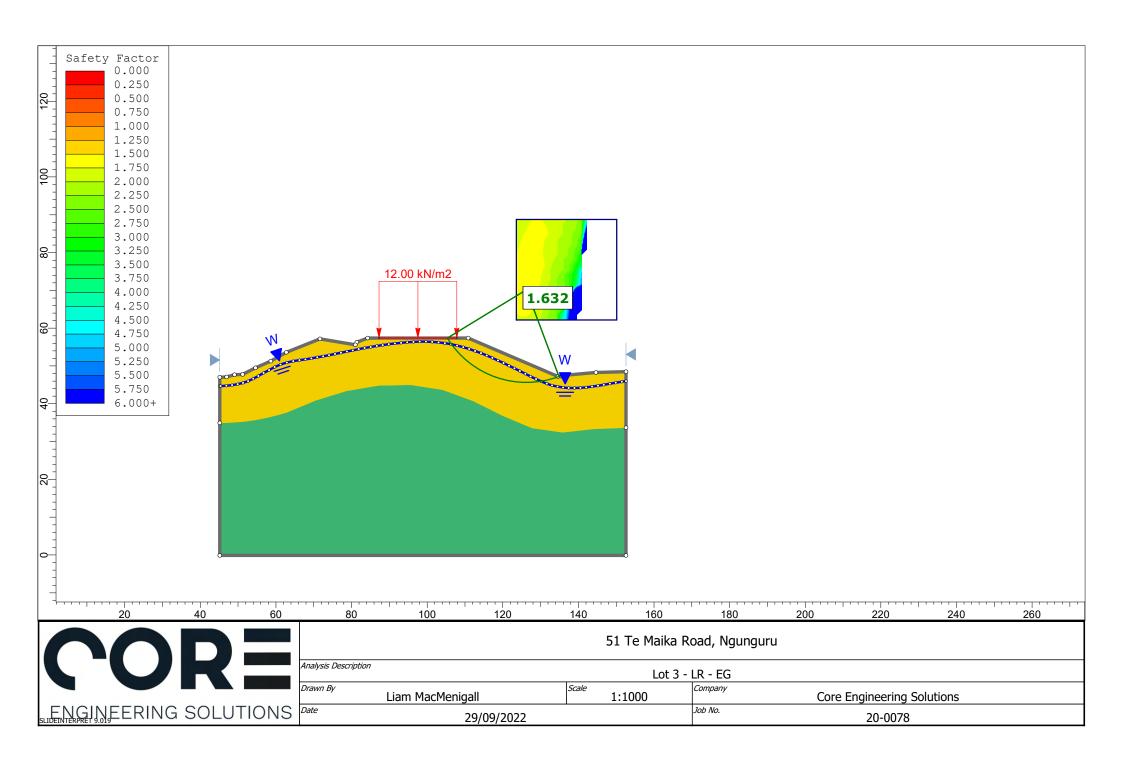


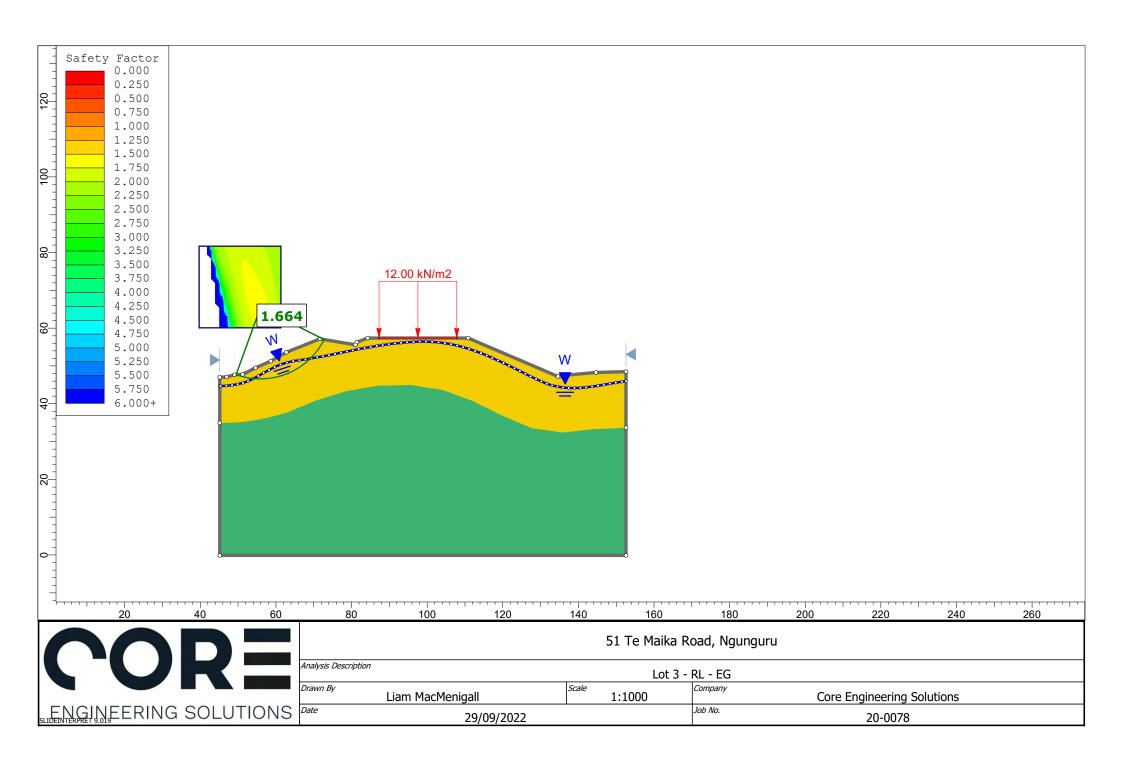
From our stability assessment, multiple sections through the site were analysed using the above parameters and design conditions set by WDC, and from this, compliant factors of safety (FoS) were achieved. From the assessment above, the following recommendations are proposed for this development;

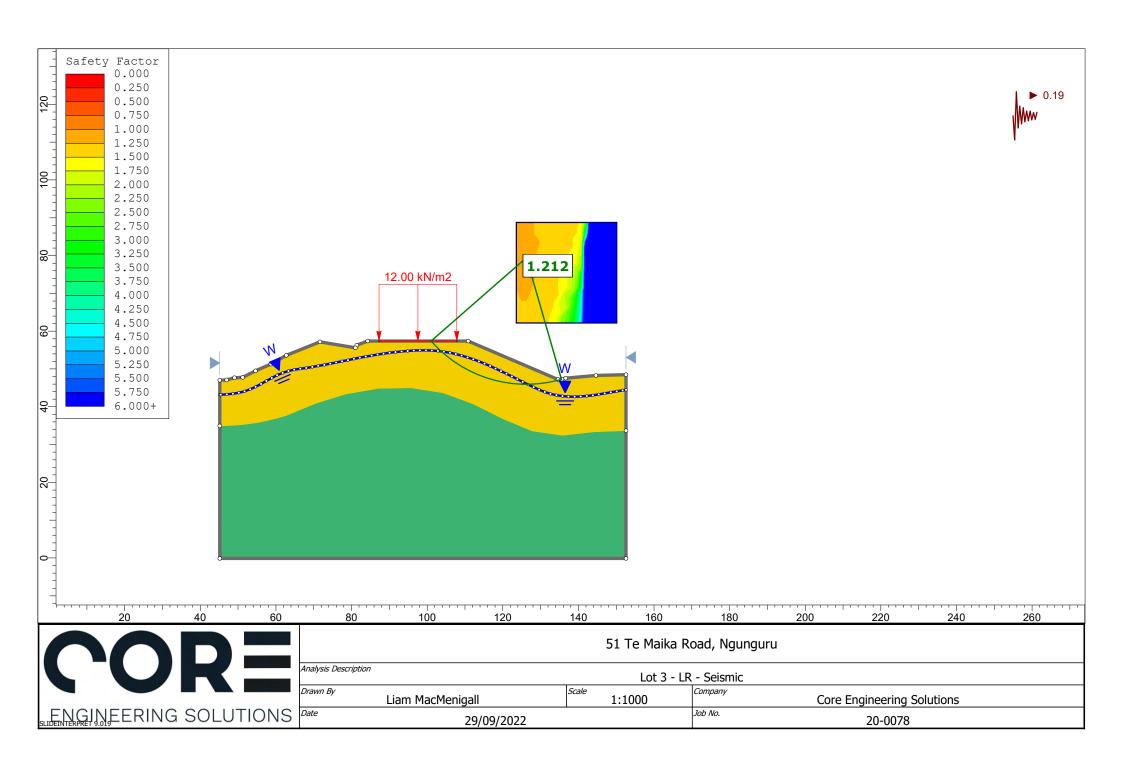
3.0m setback to the ridgeline flanks to any buildings within this stage unless further site-specific assessment is undertaken by a Geo-Professional. (Ref: Appendix 4)

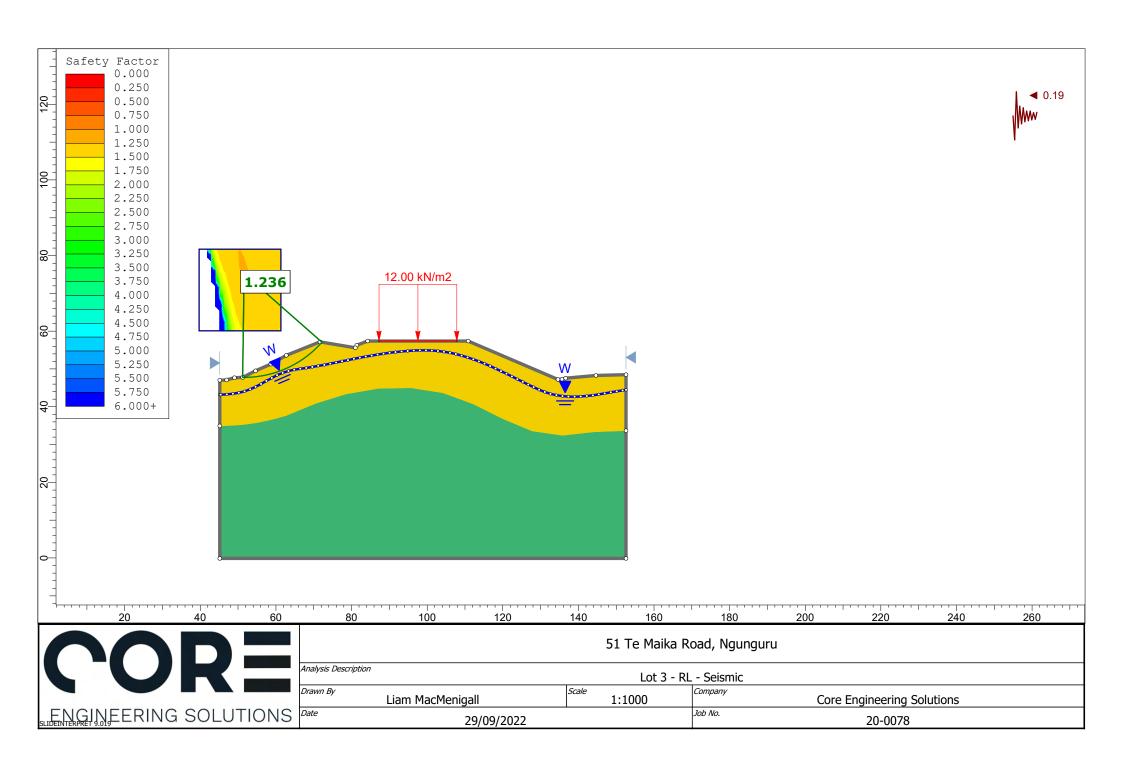


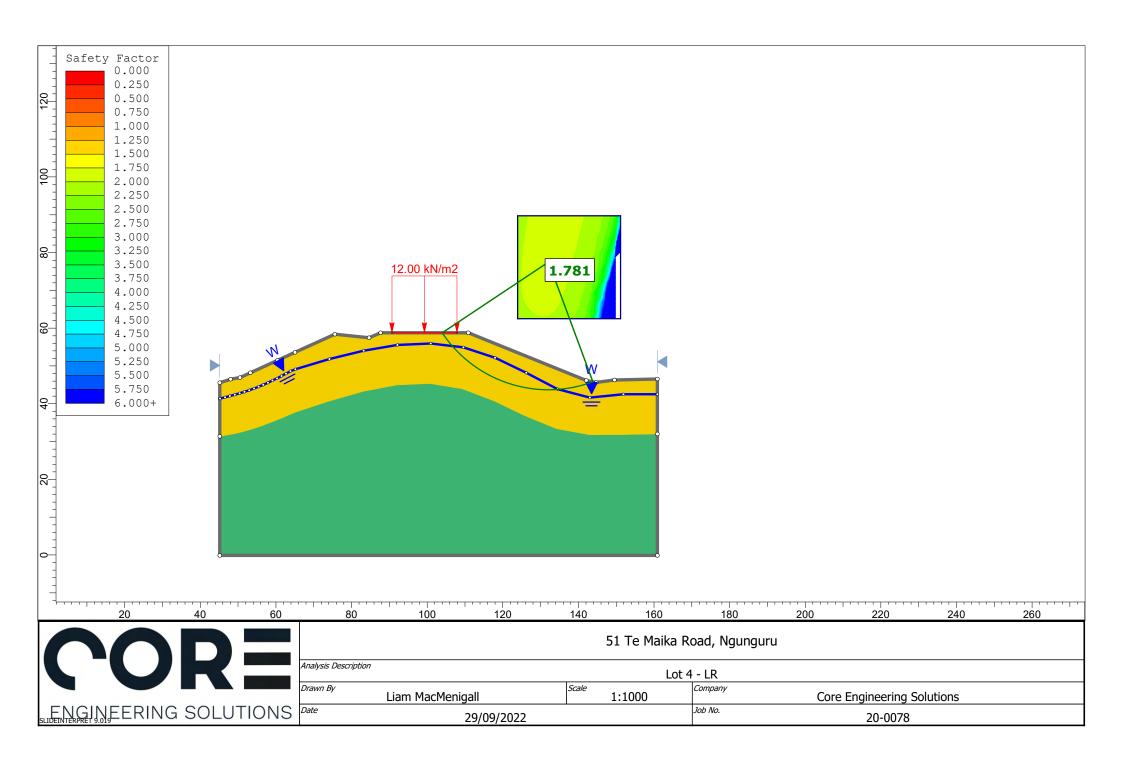


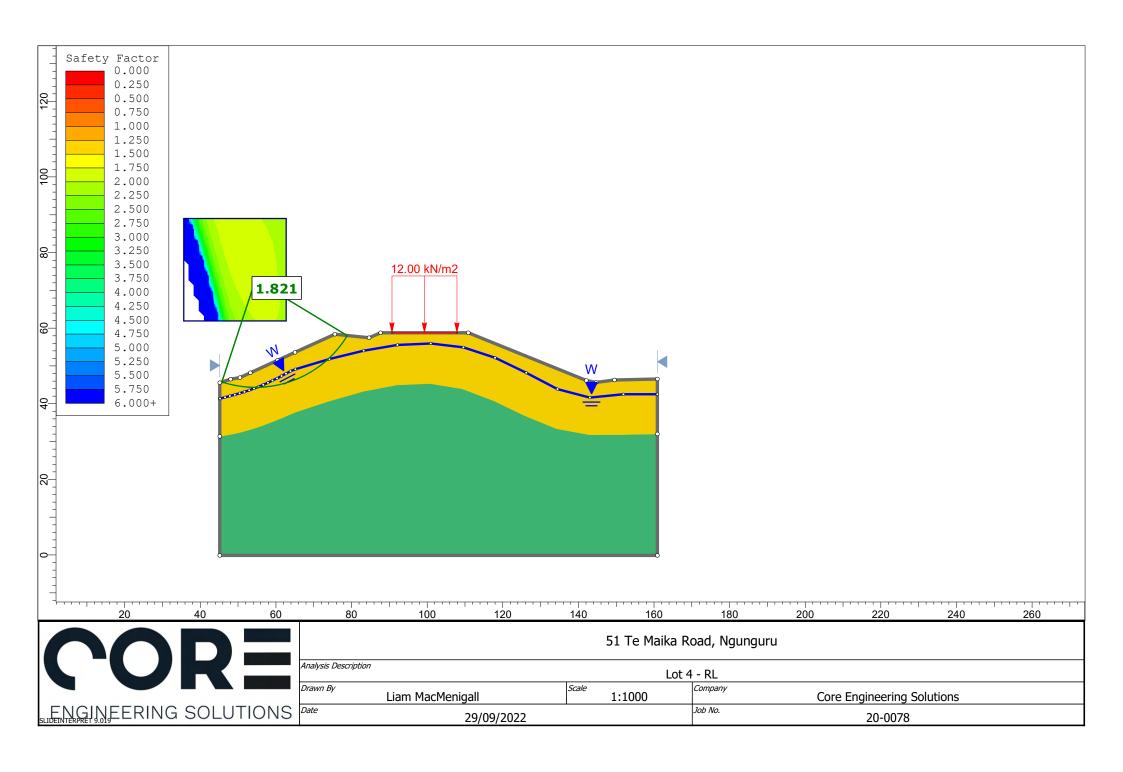


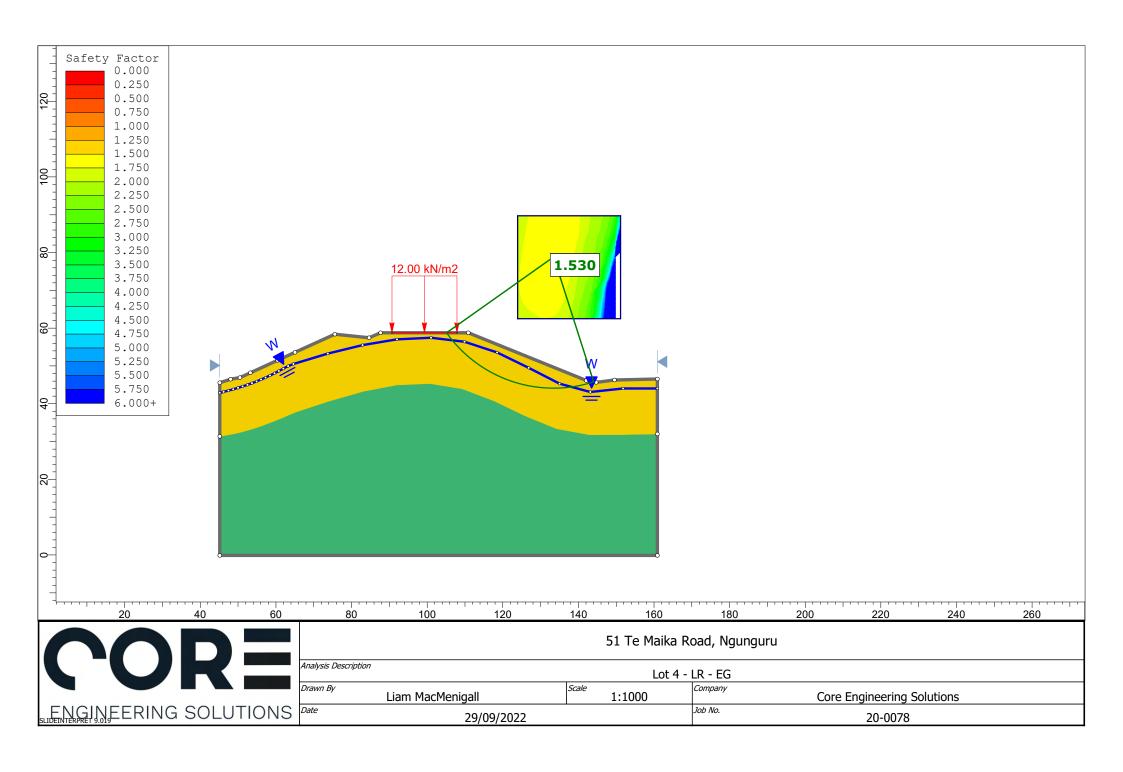


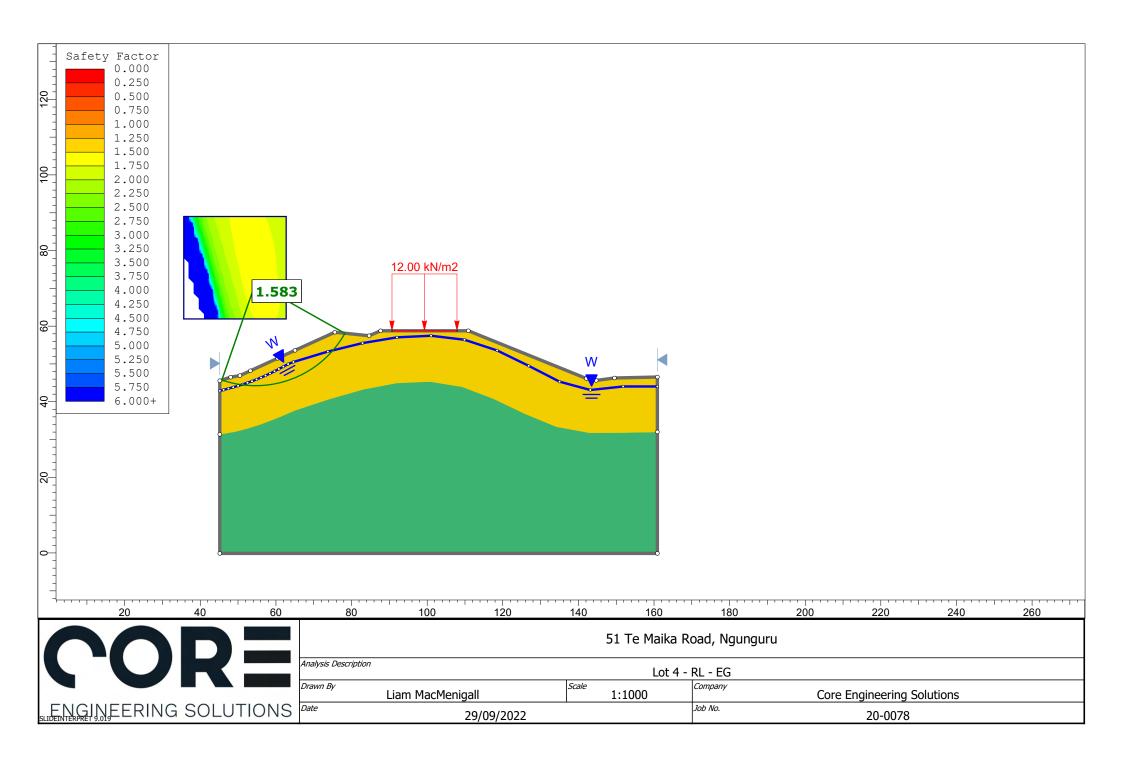


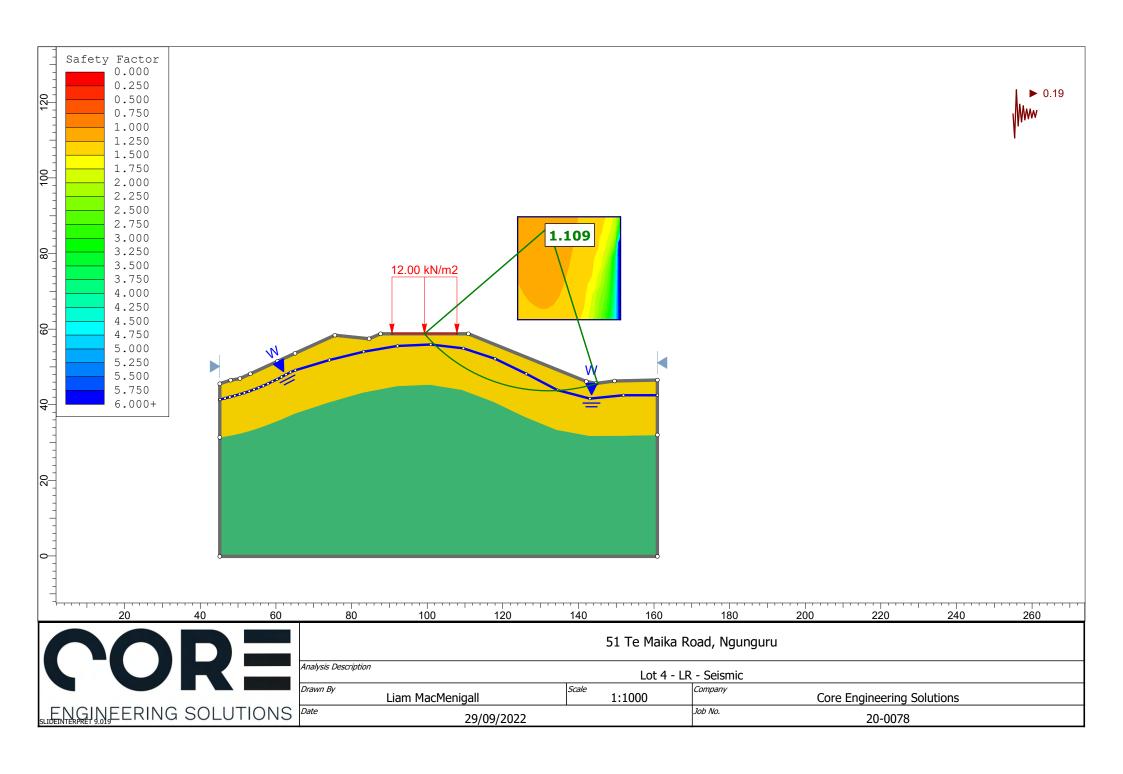


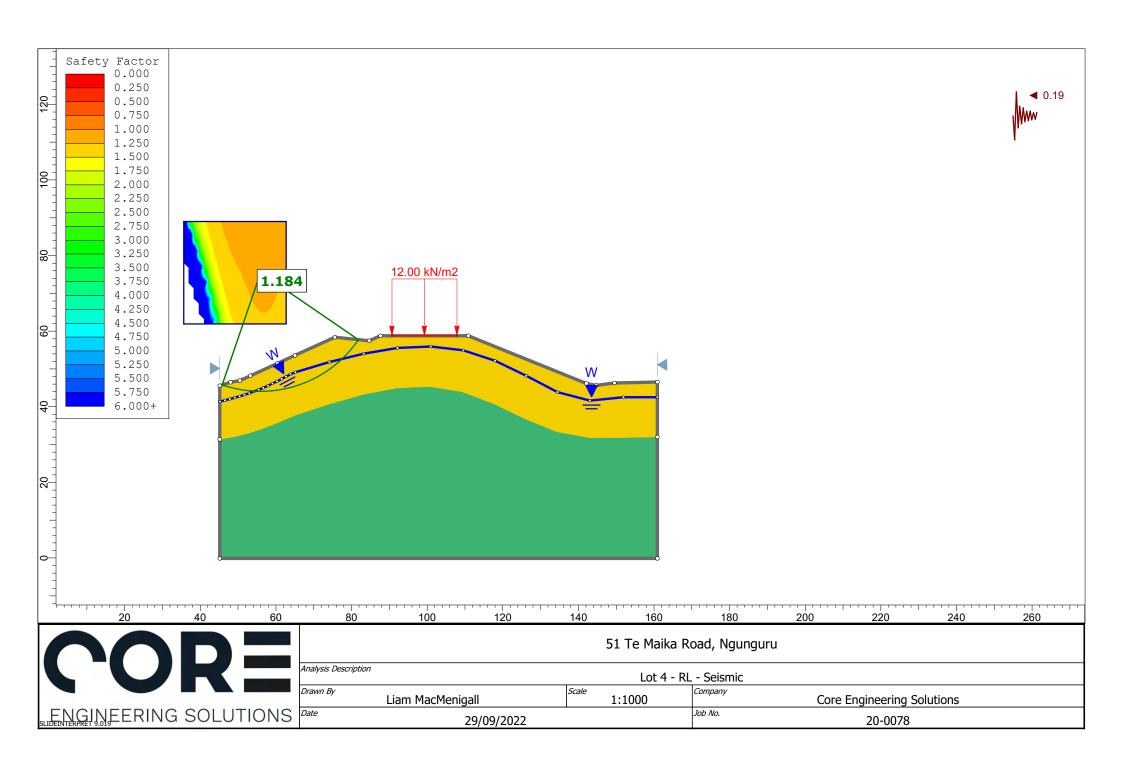


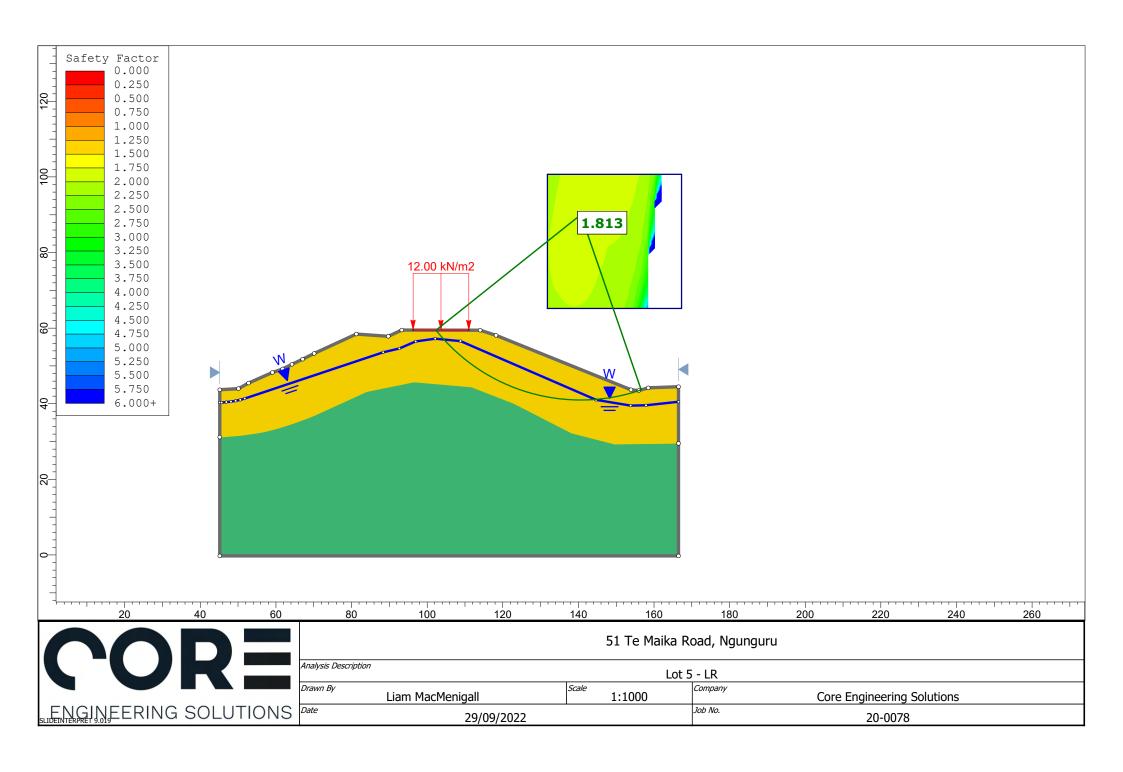


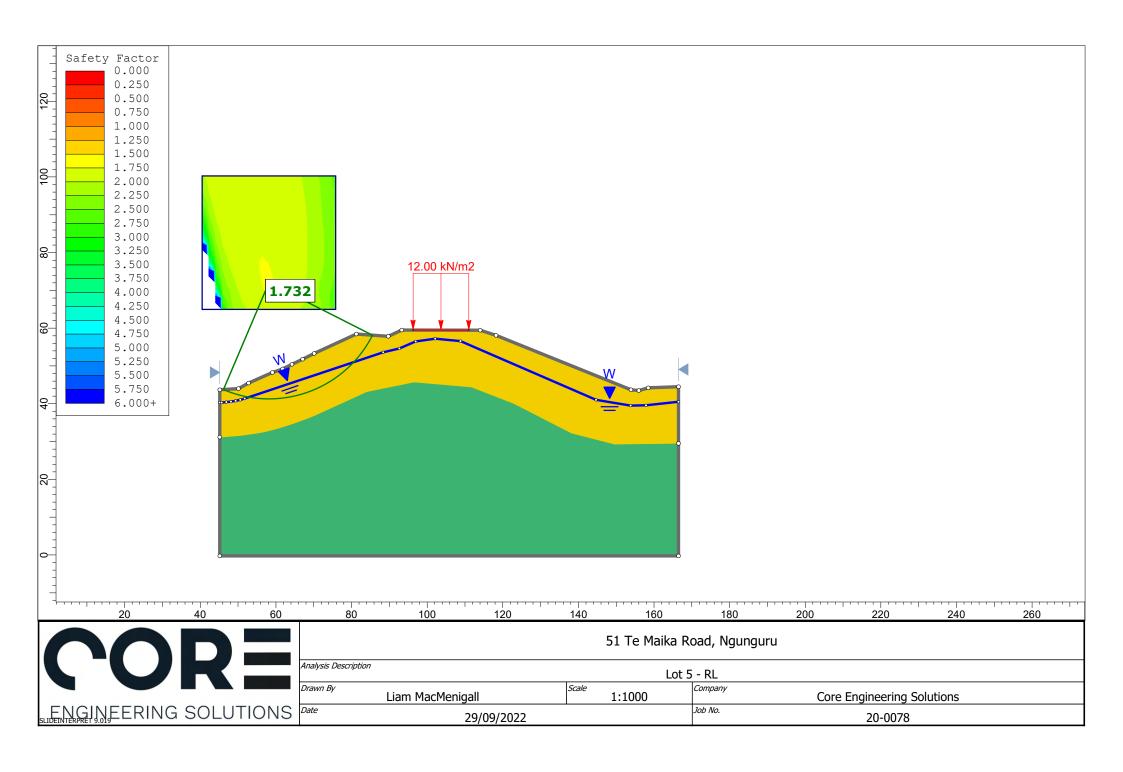


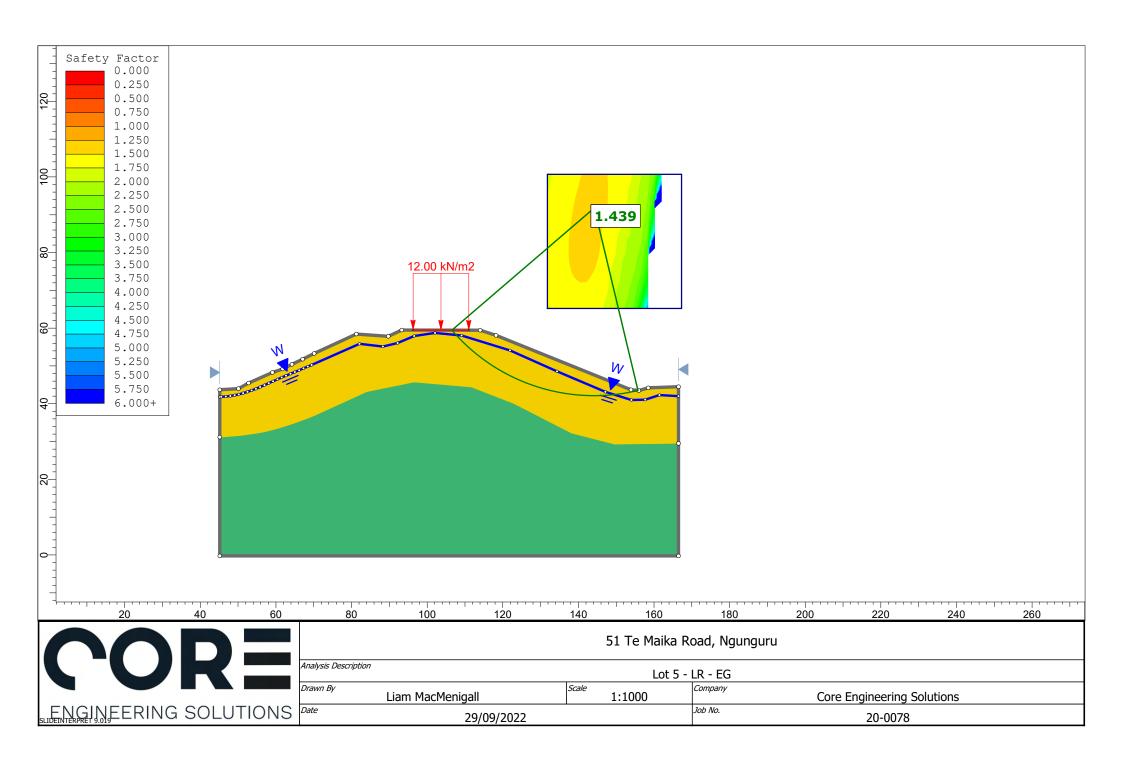


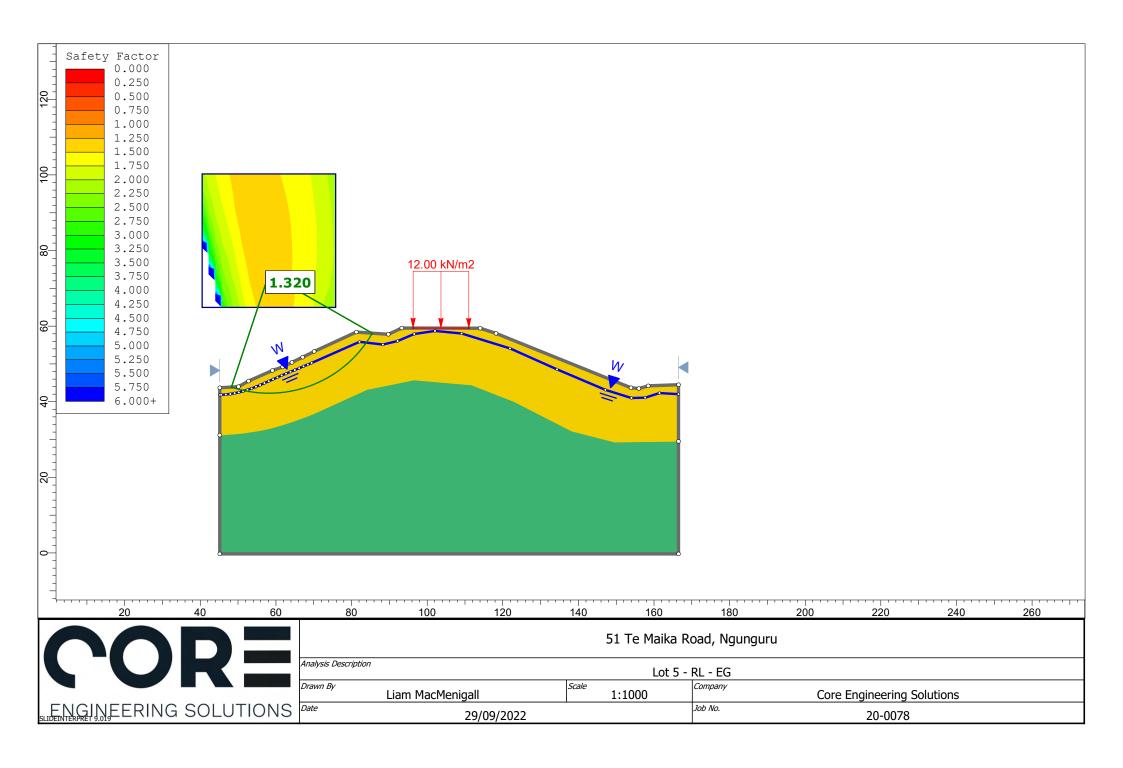


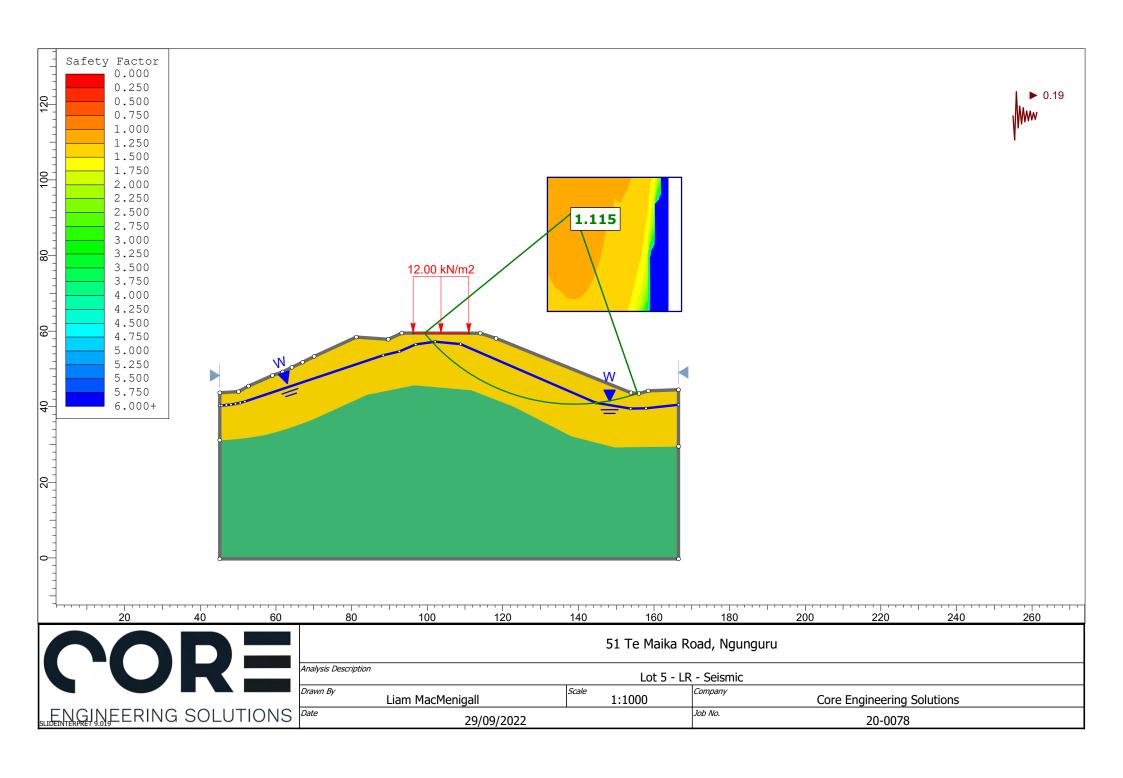


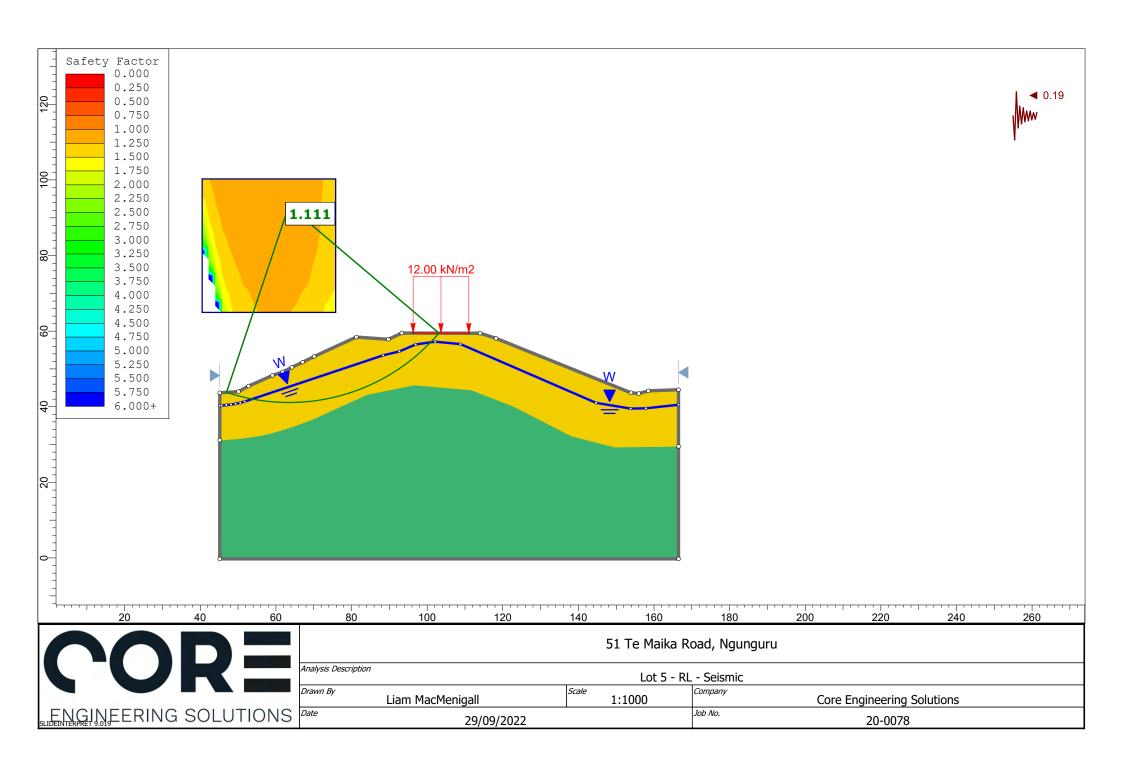


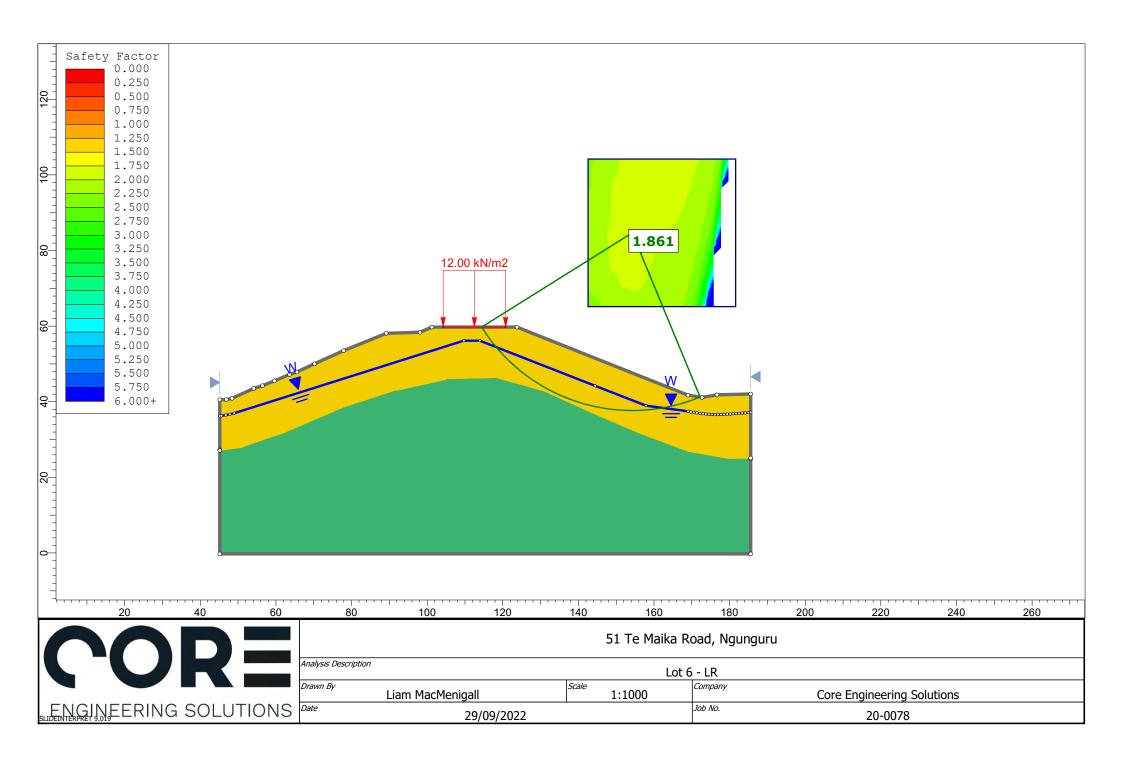


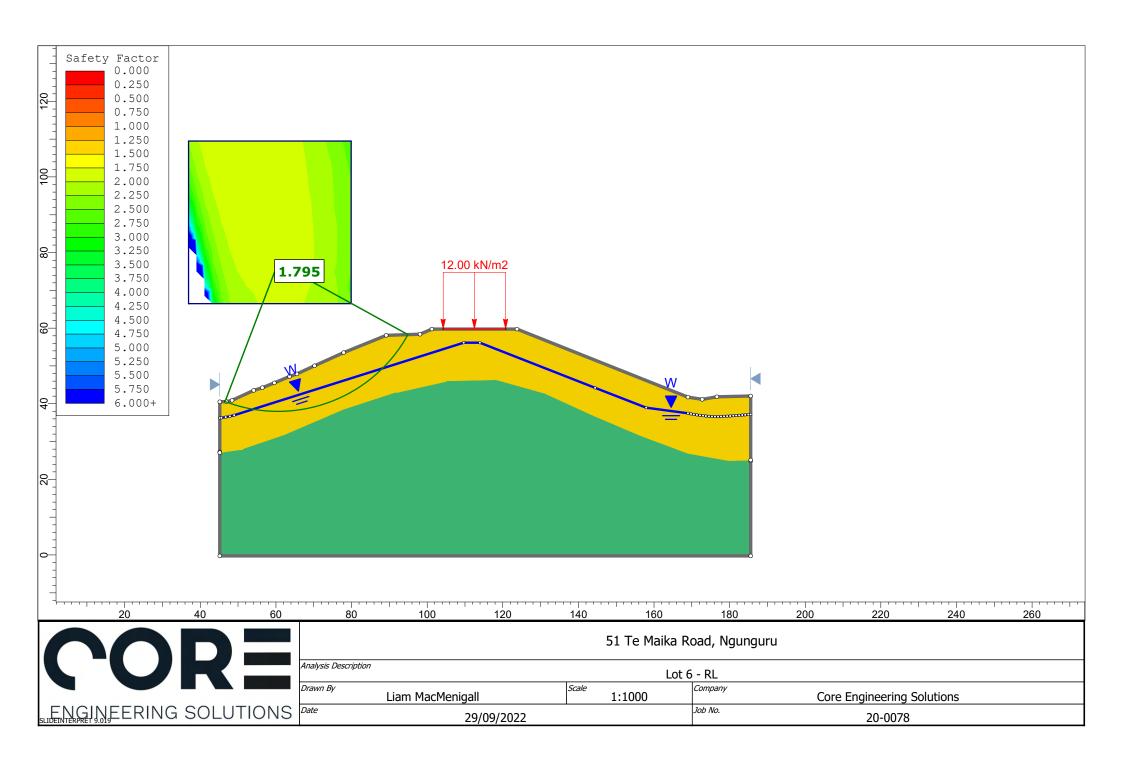


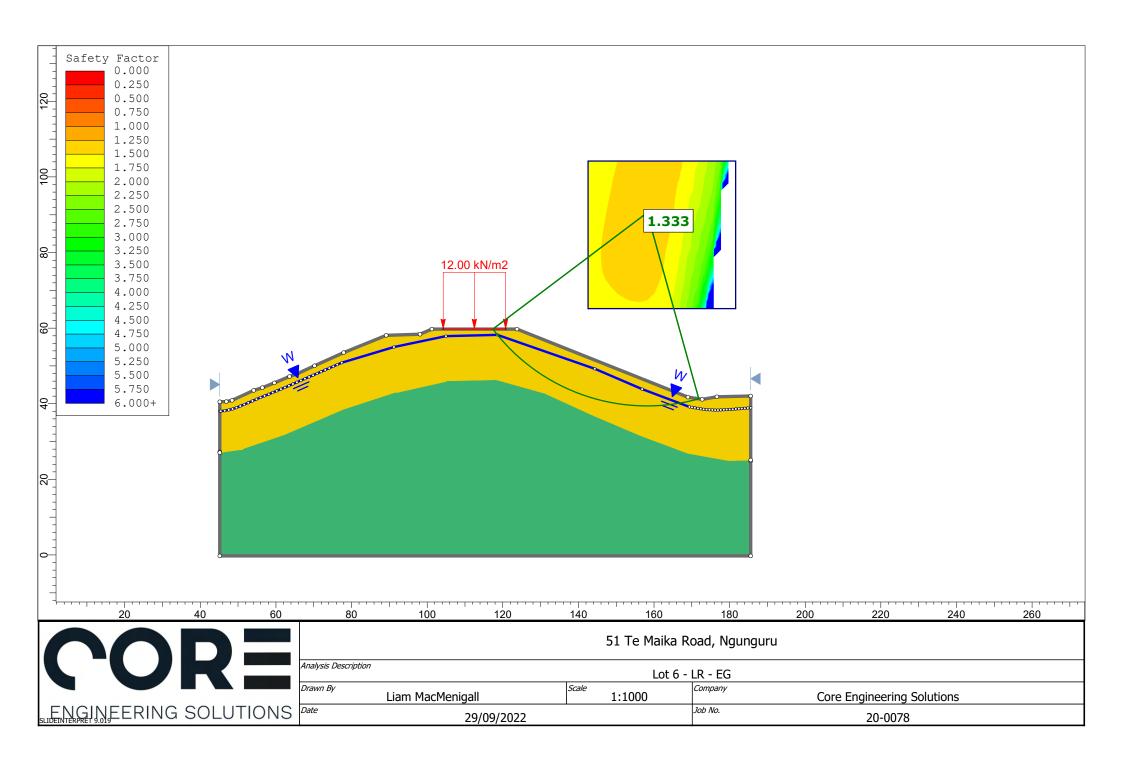


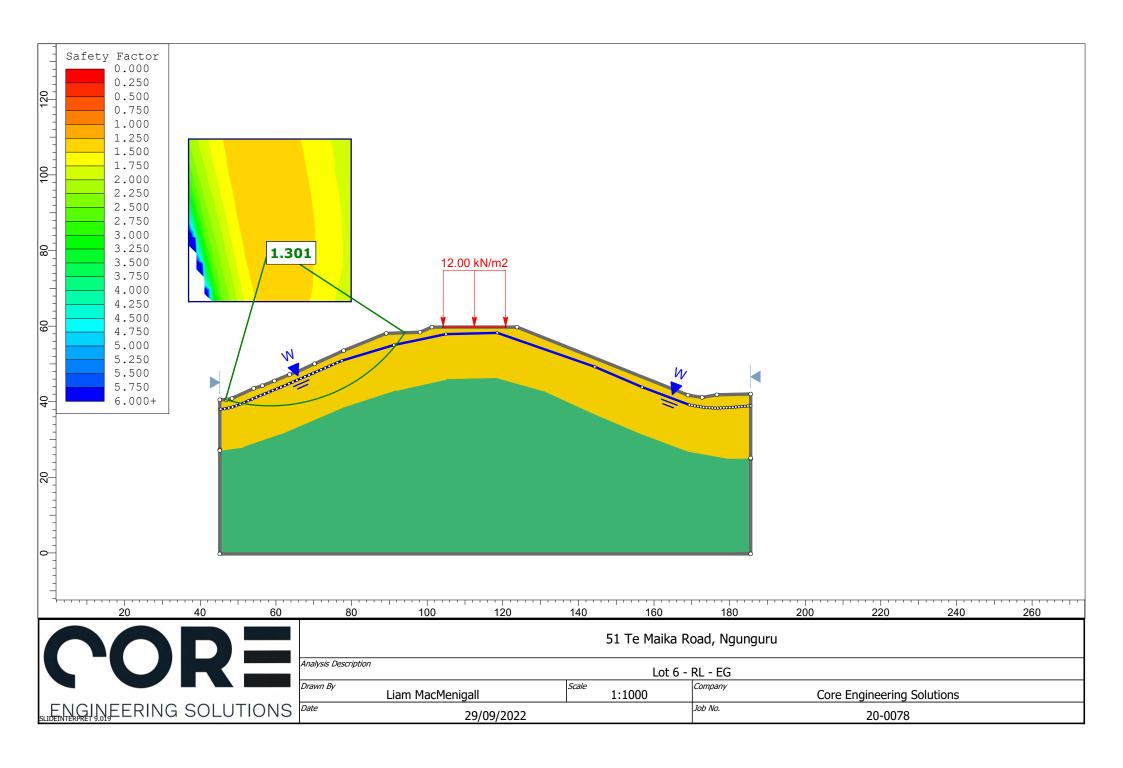


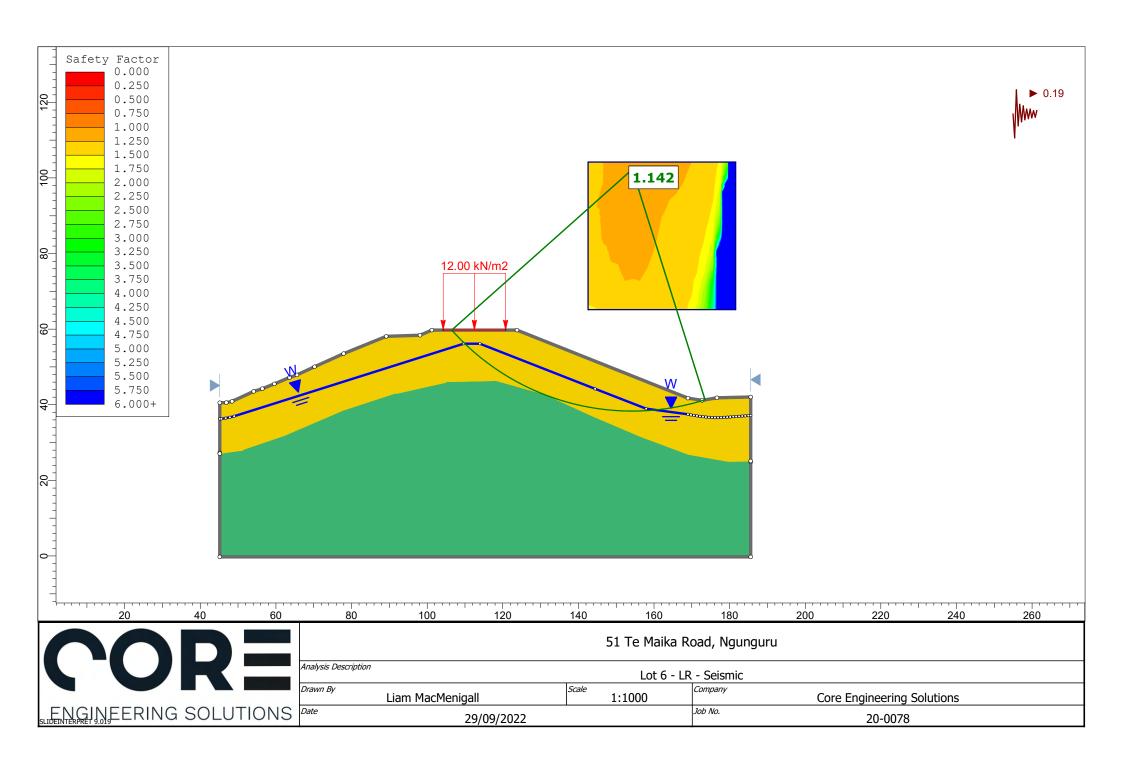


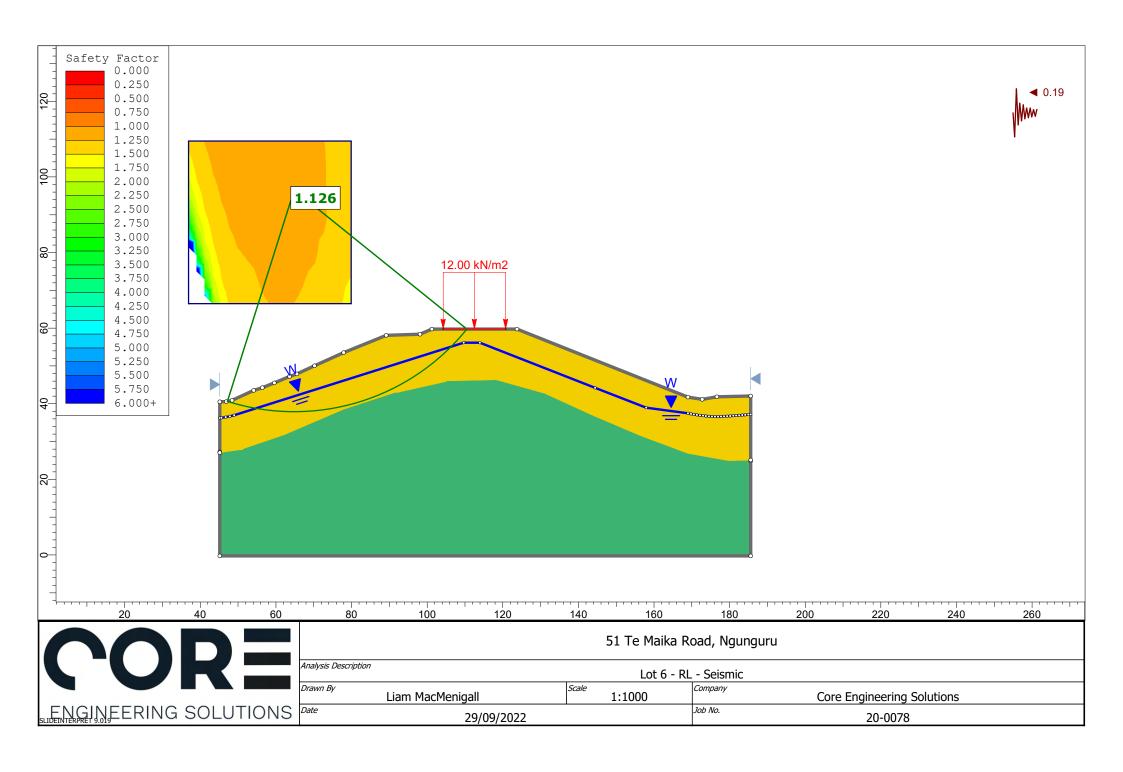


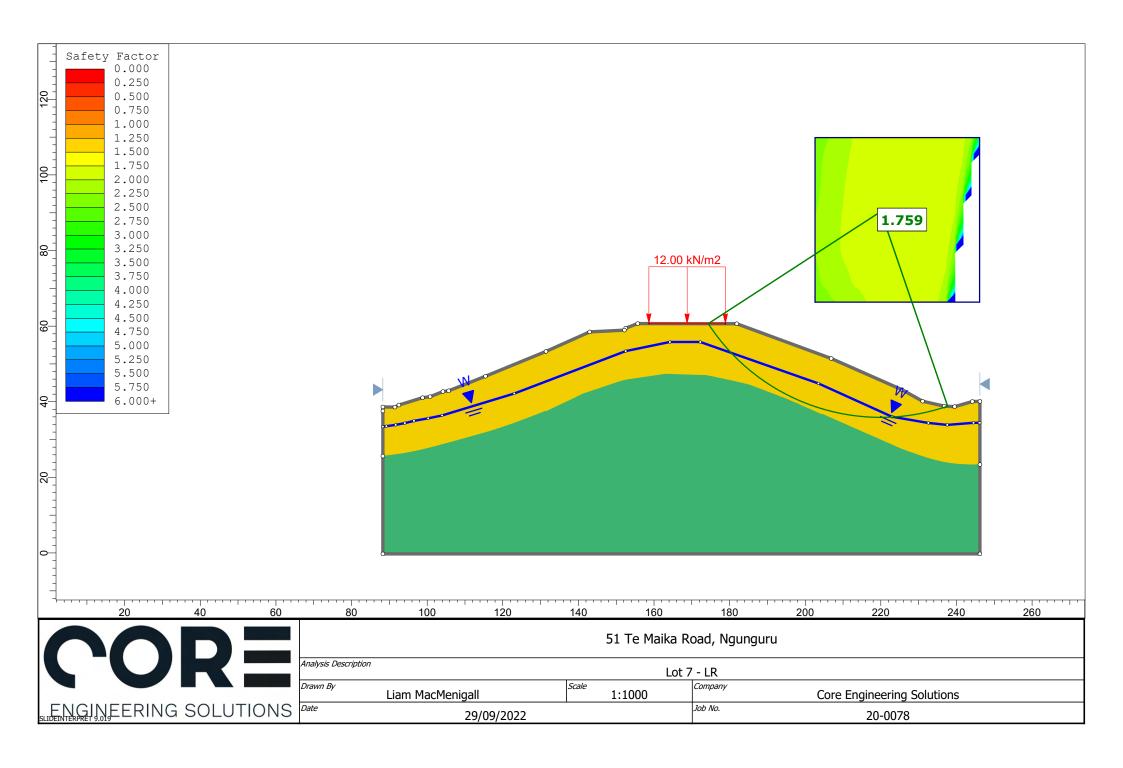


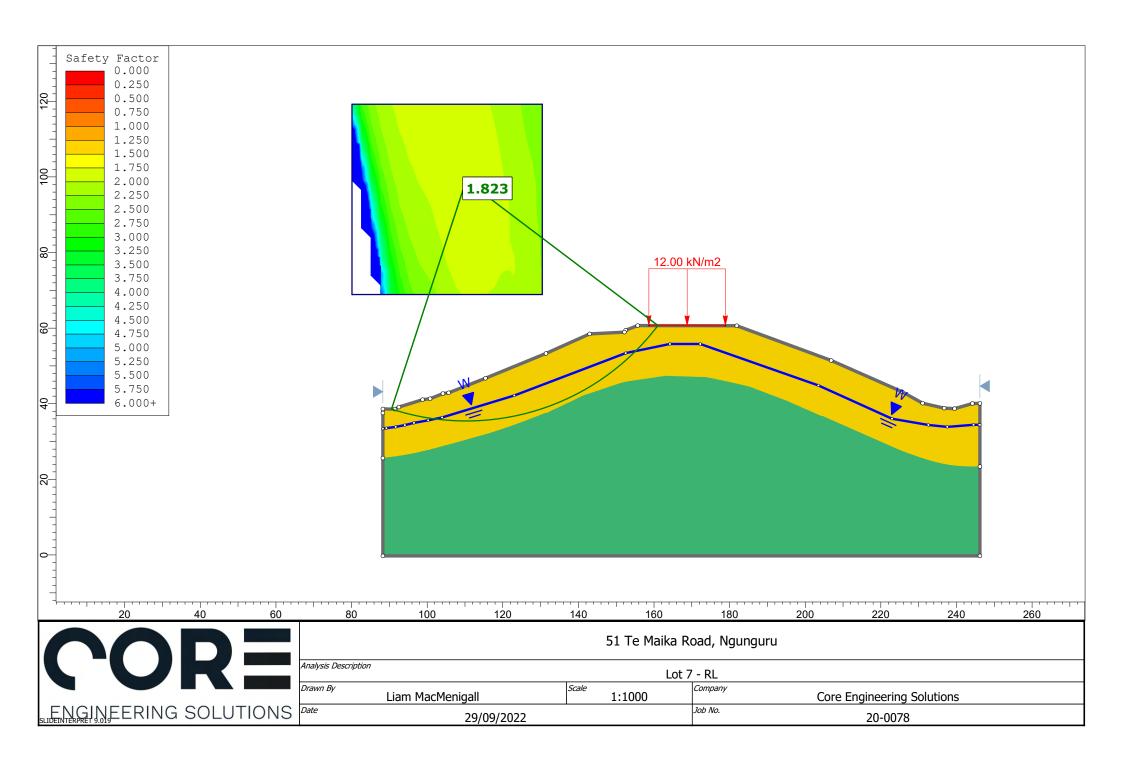


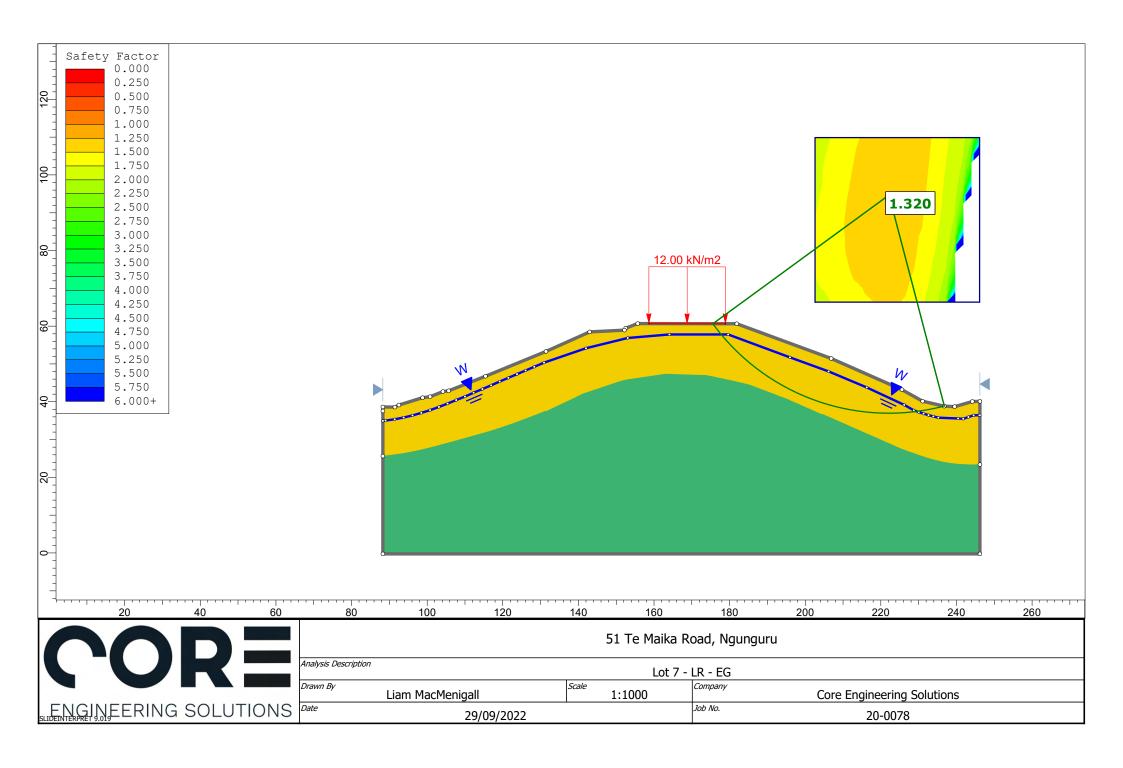


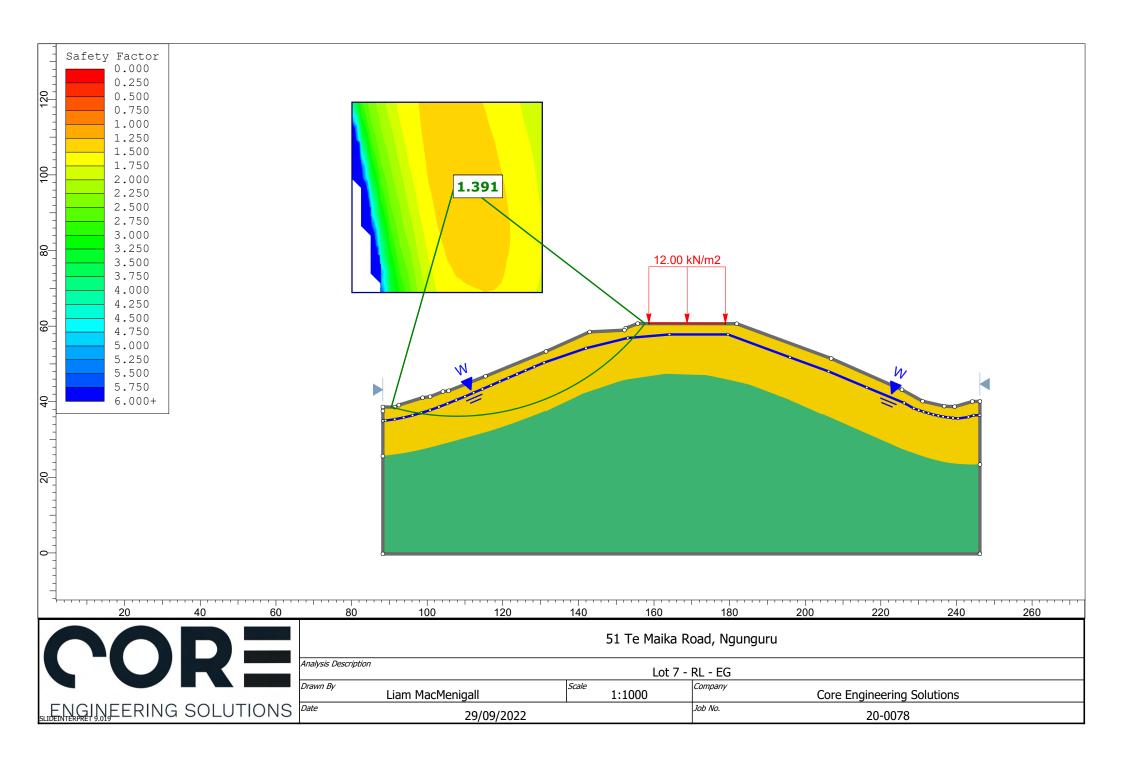


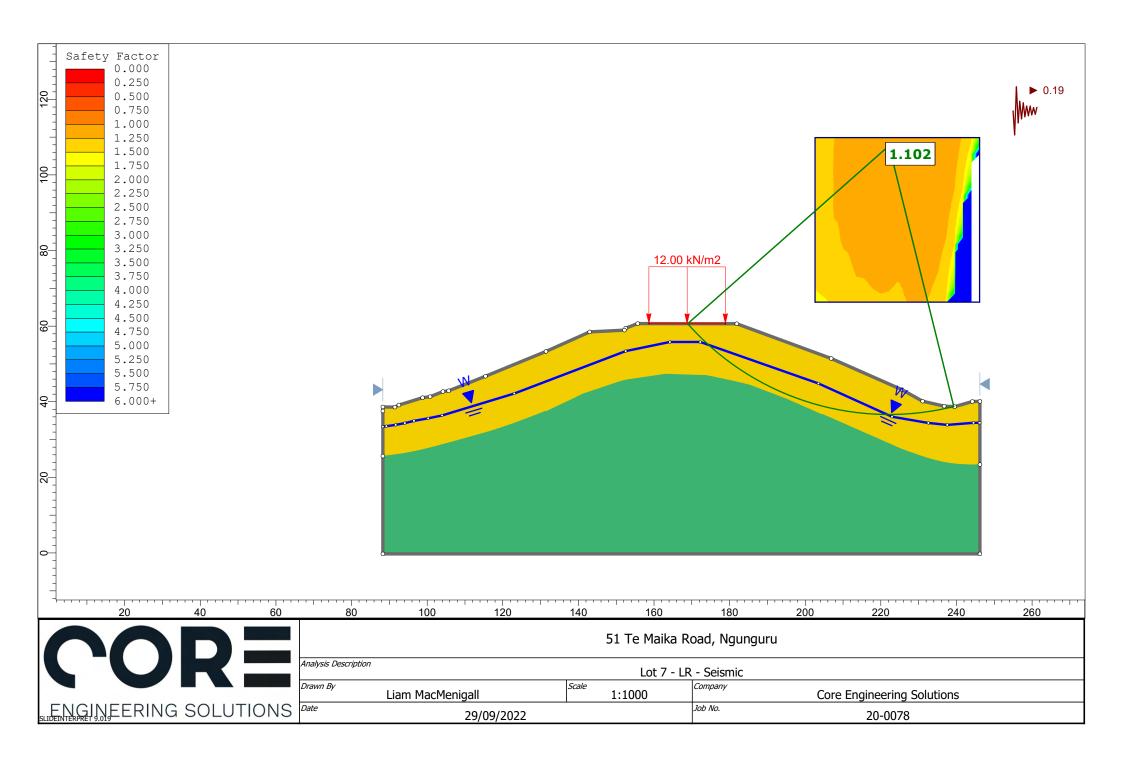


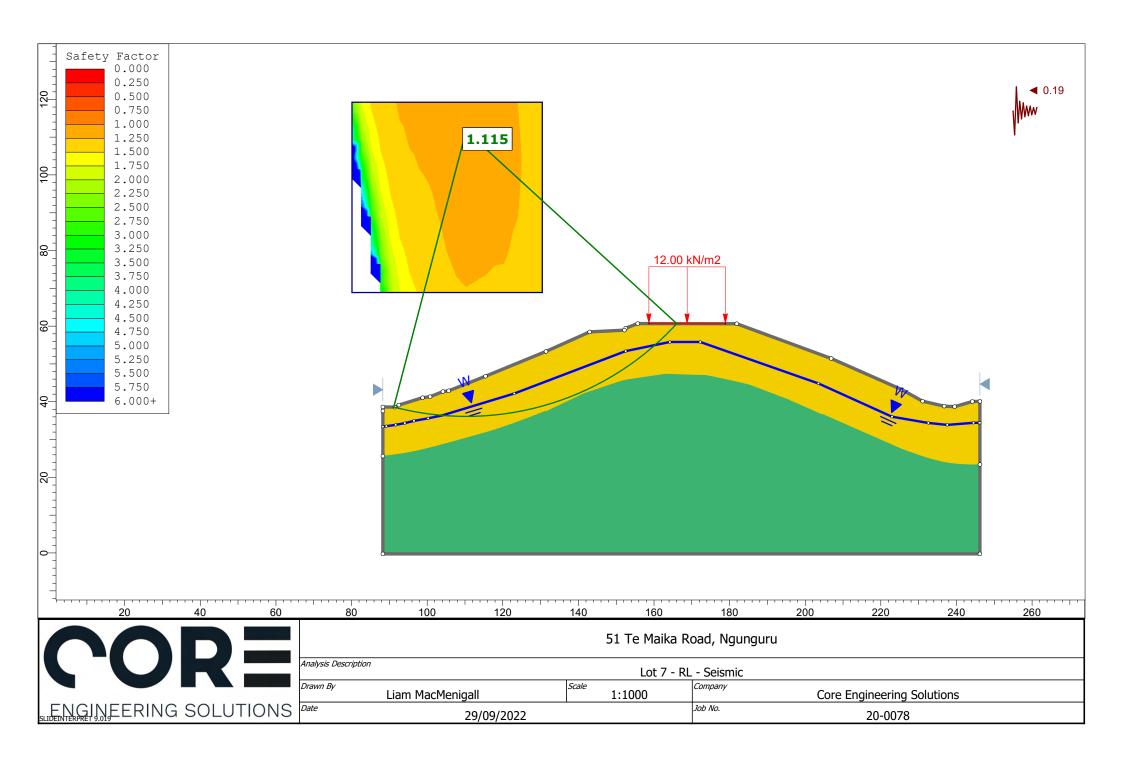


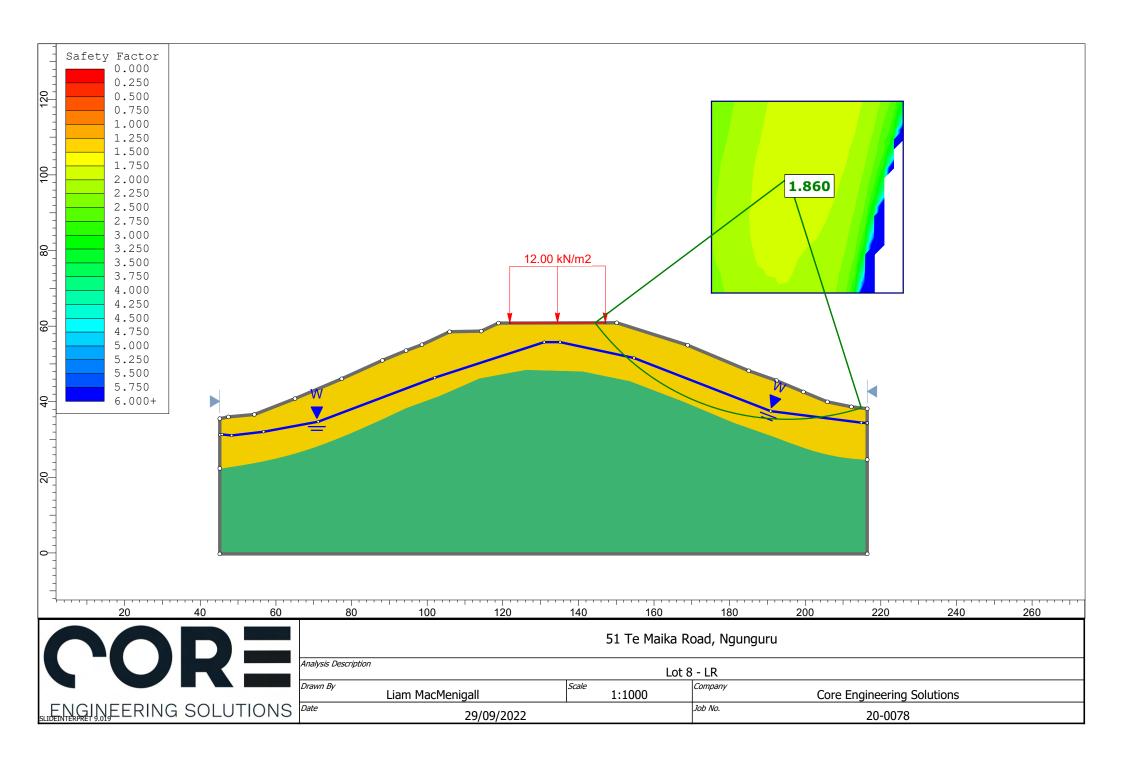


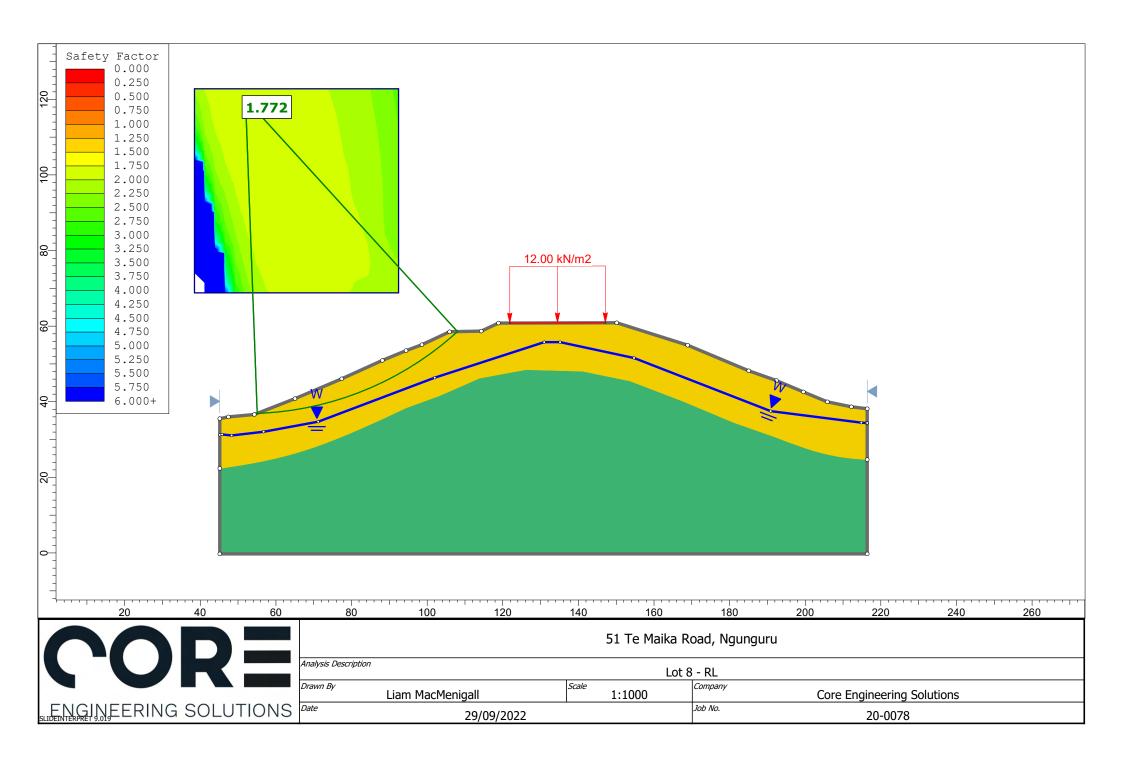


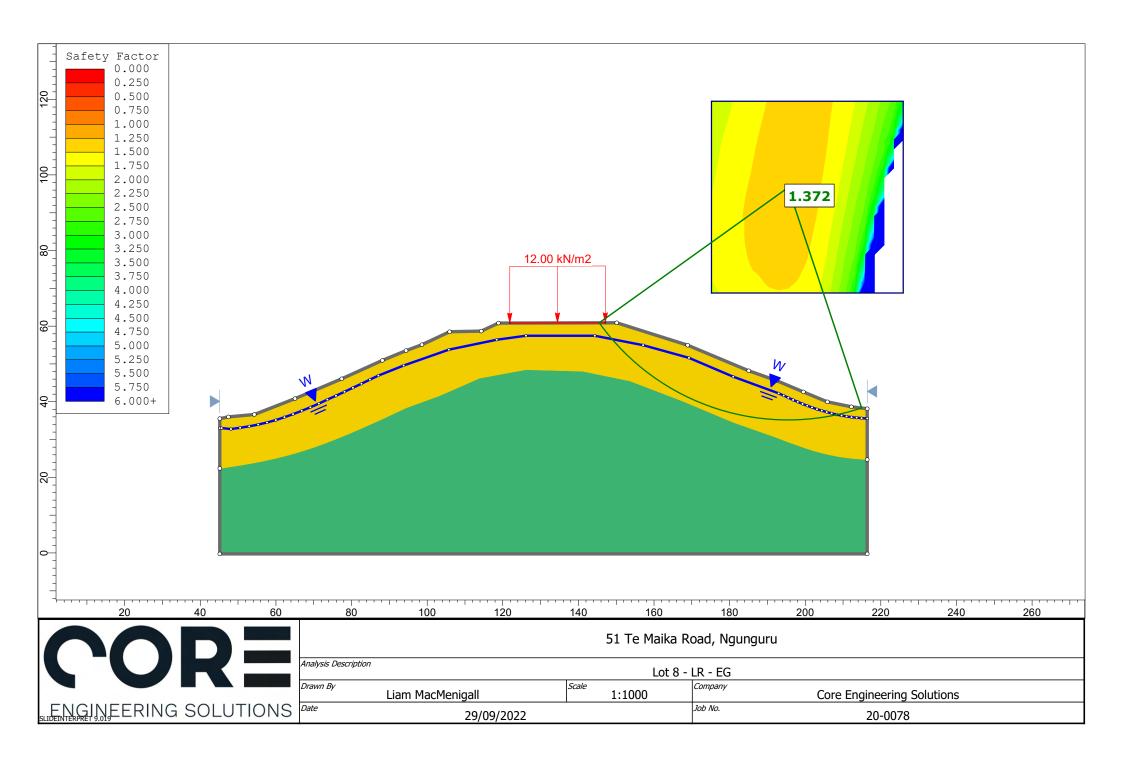


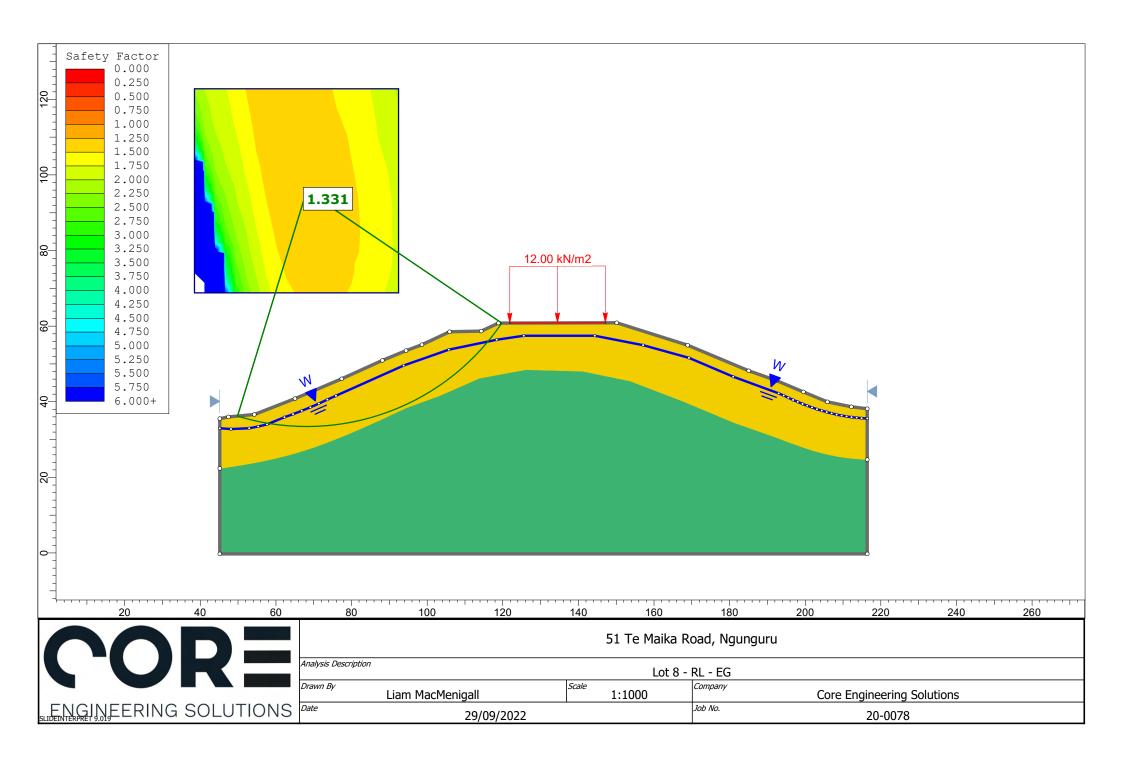


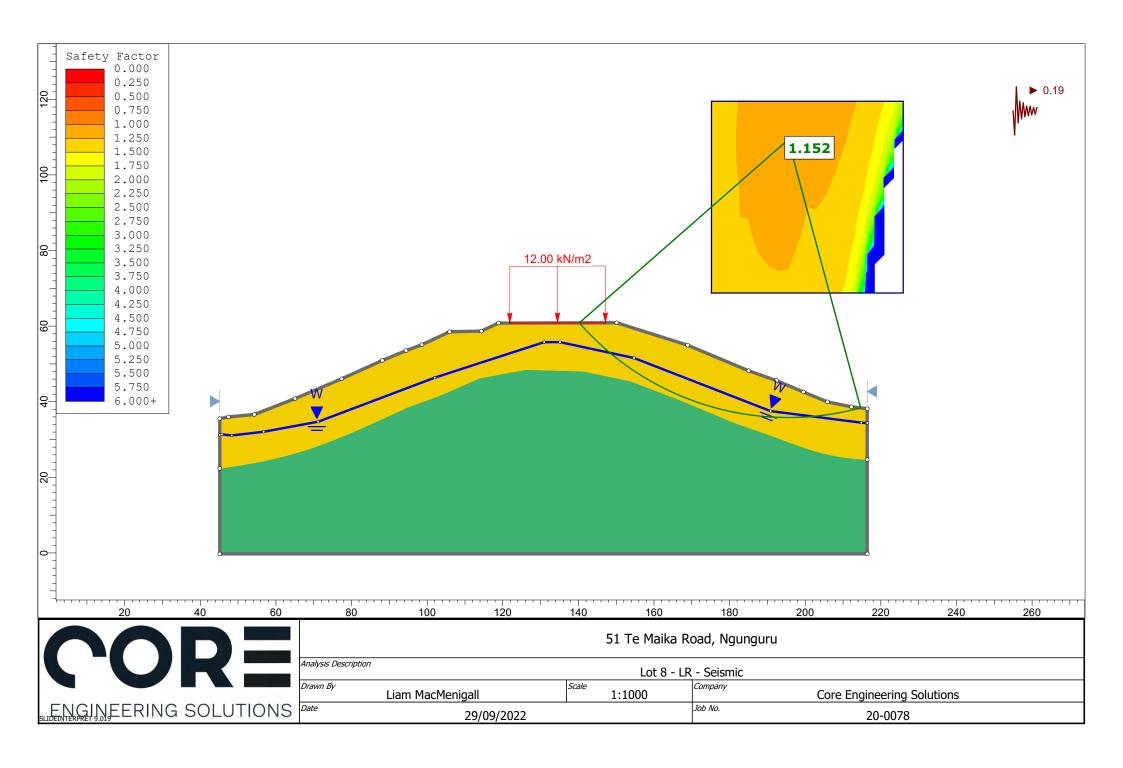


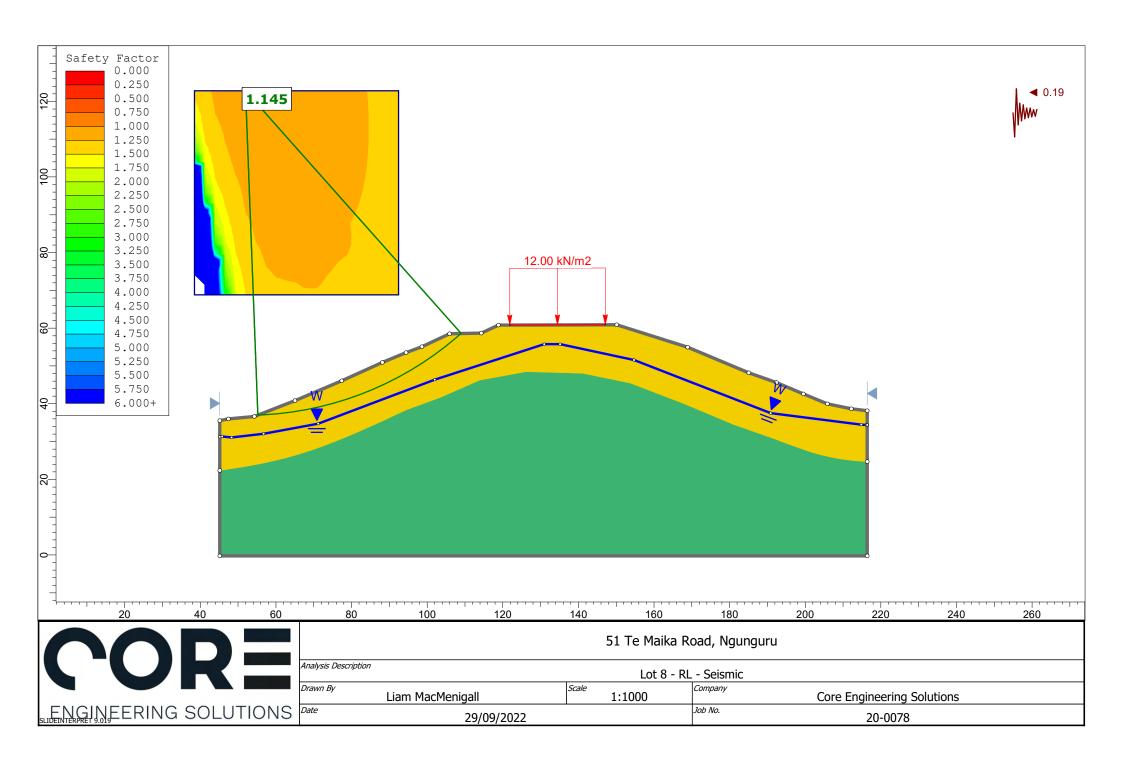


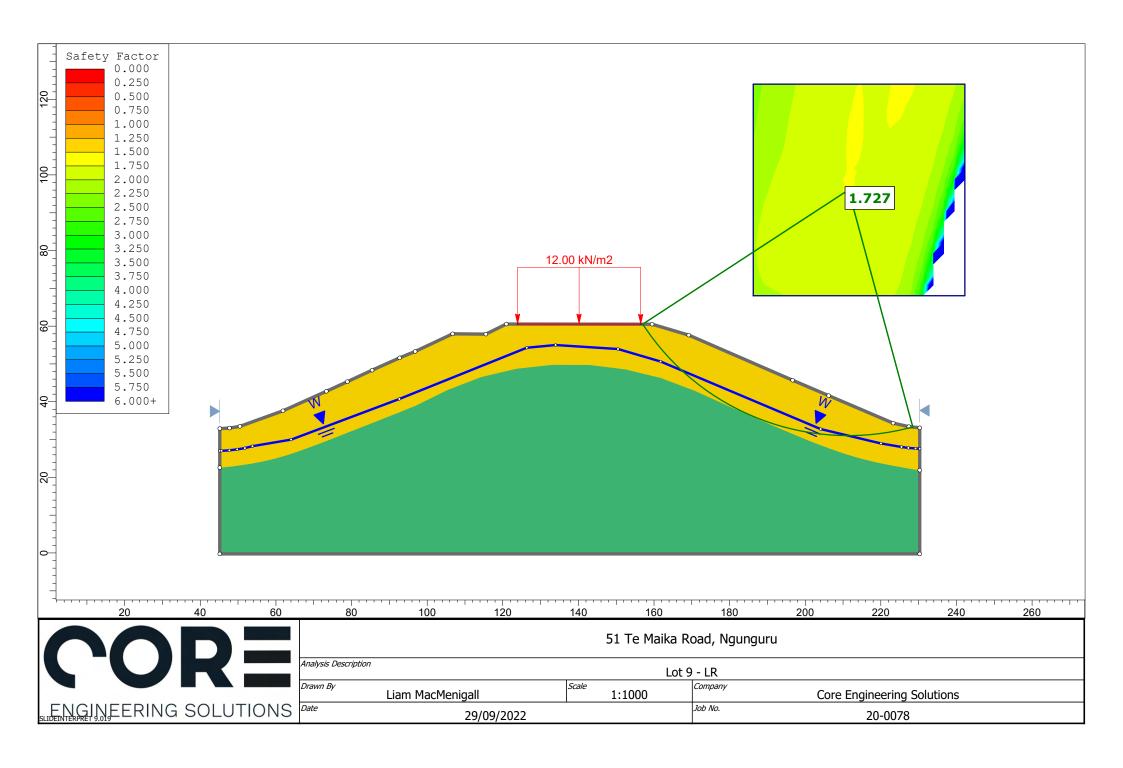


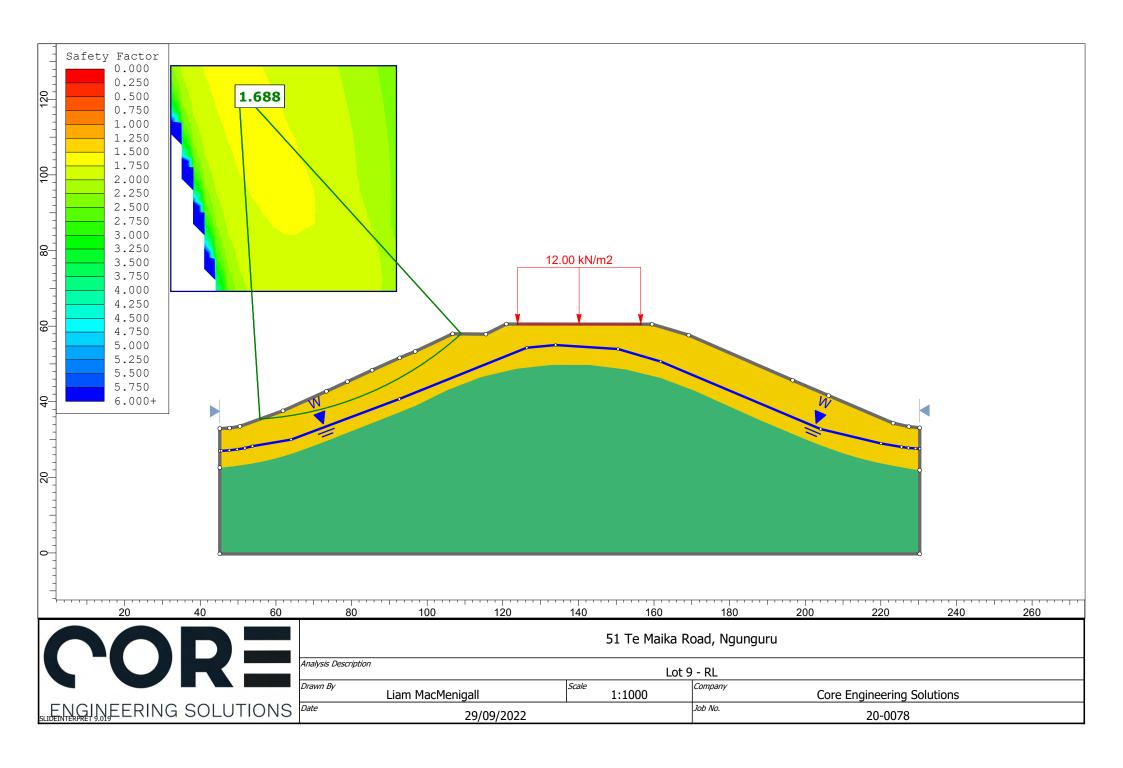


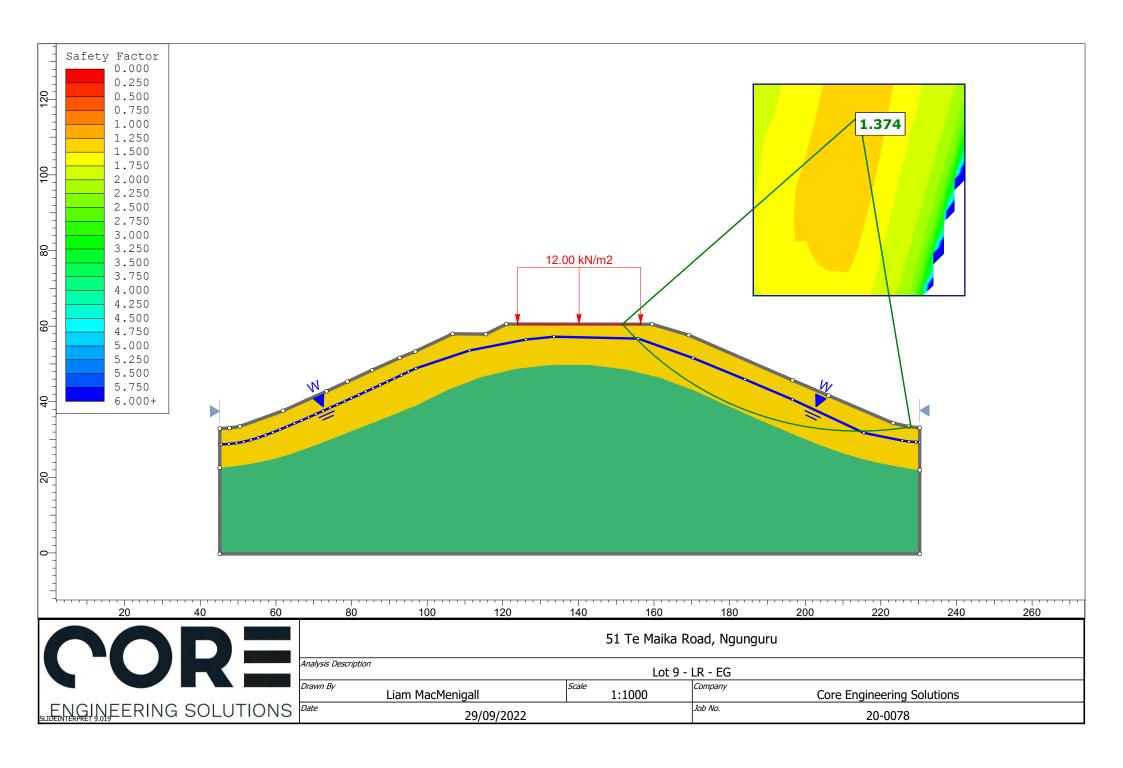


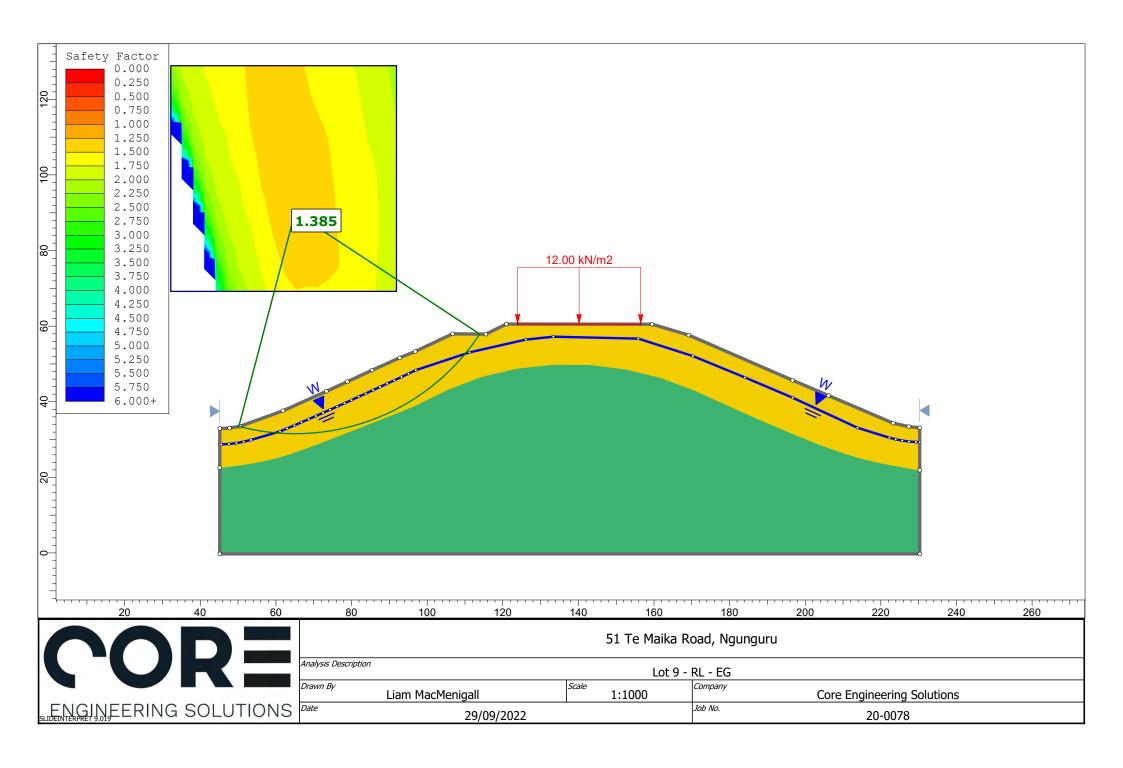


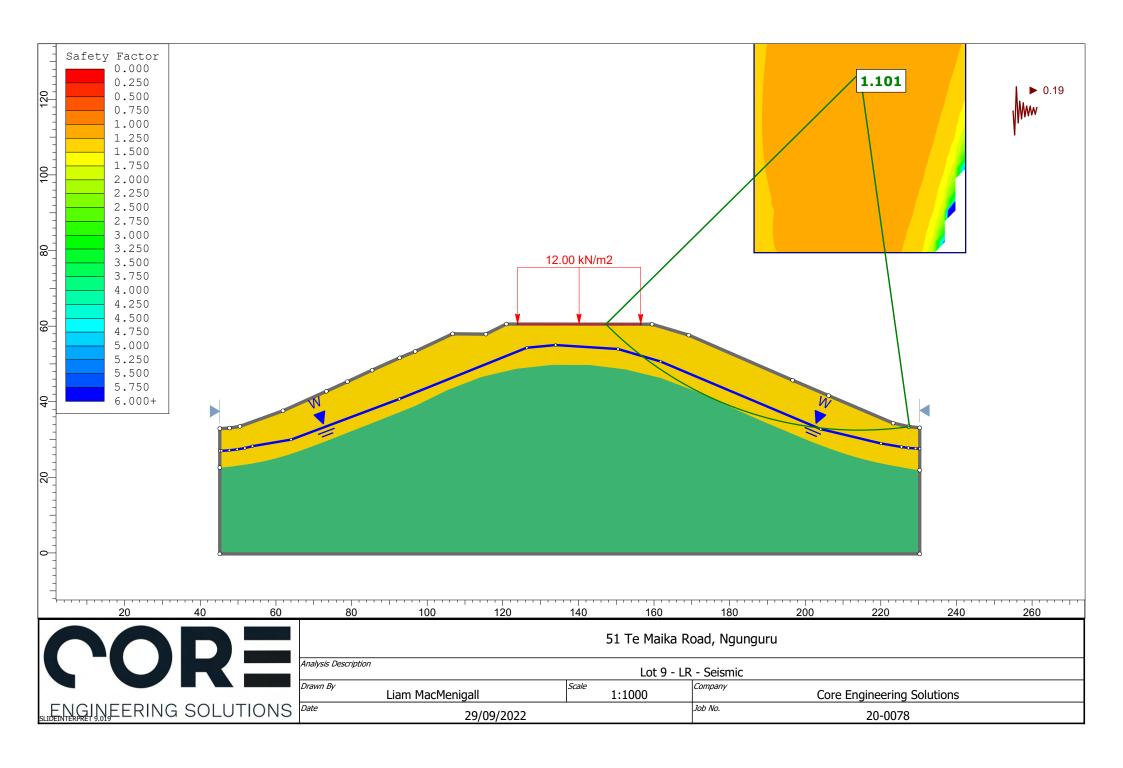


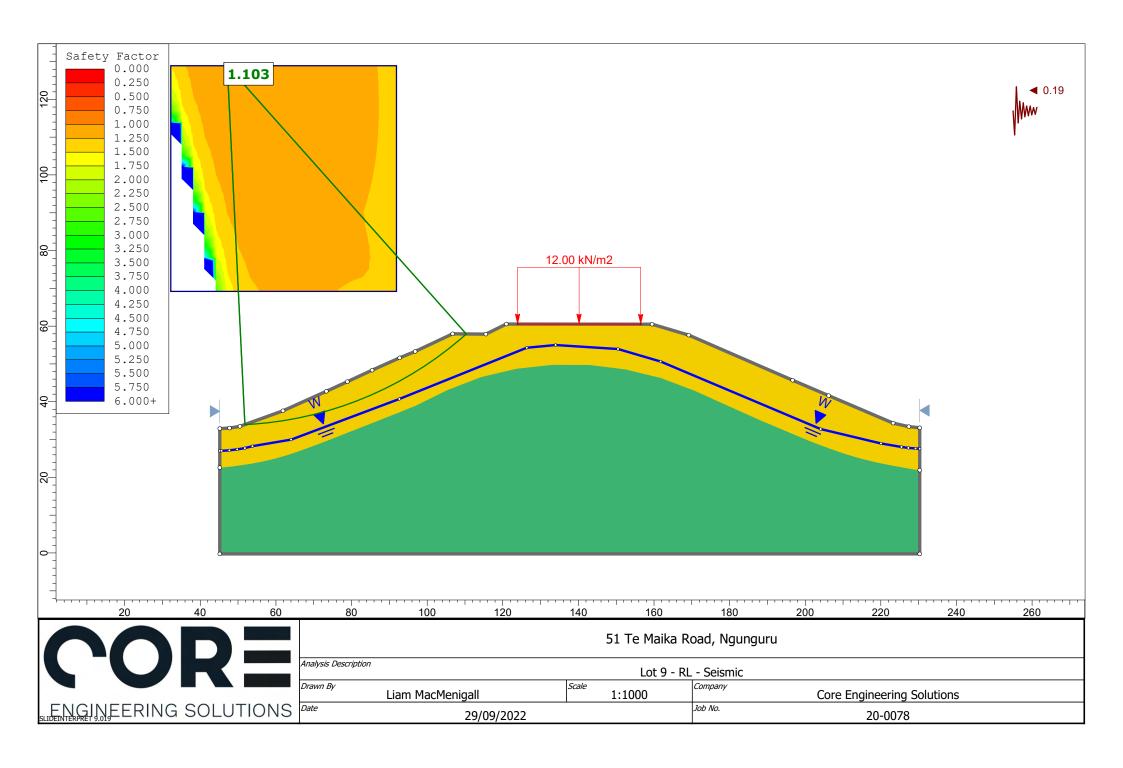


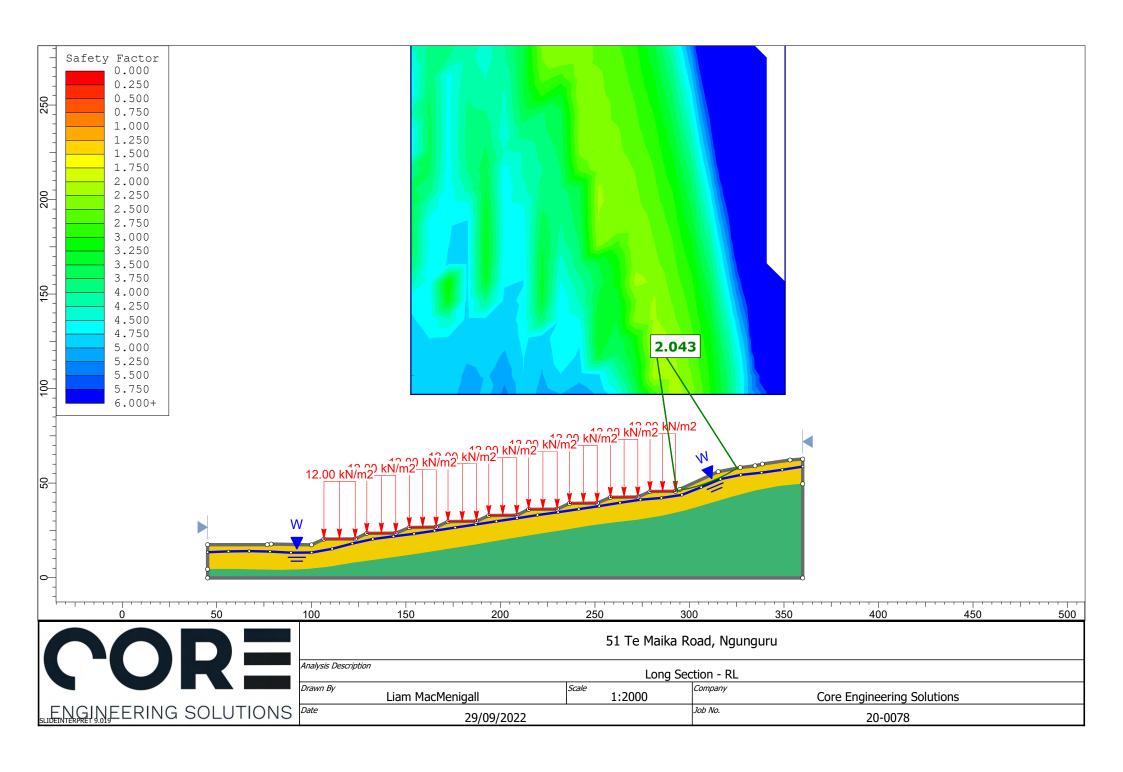


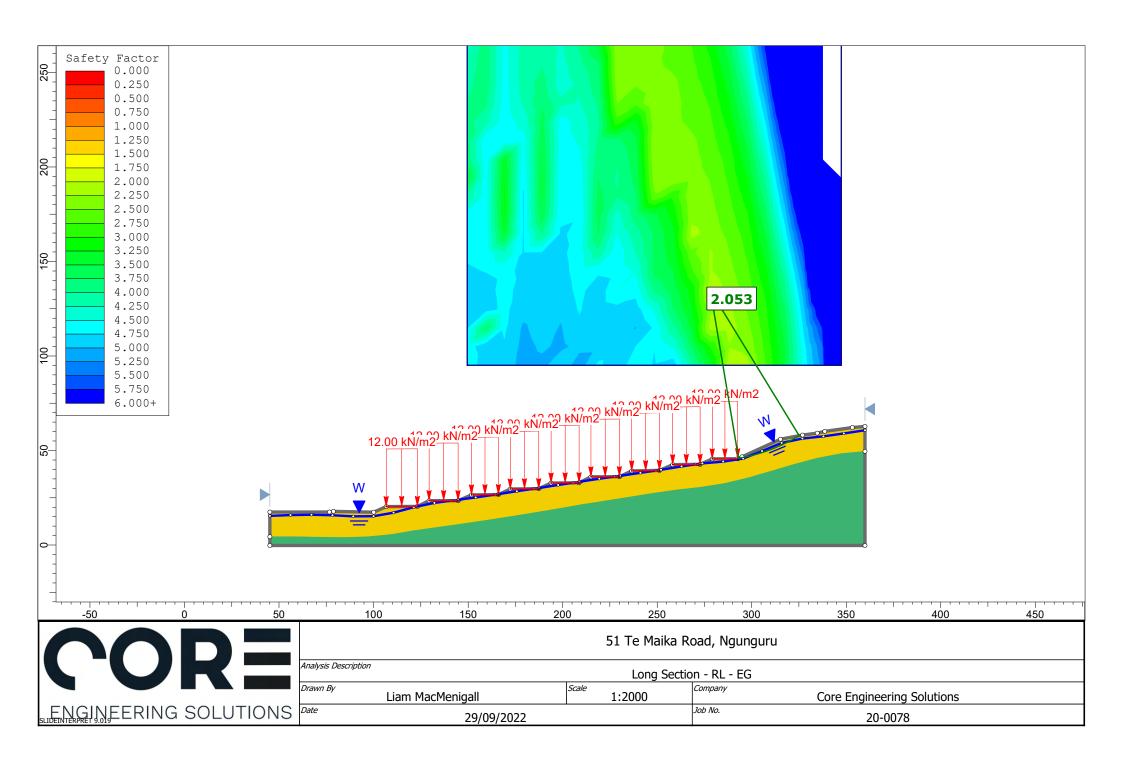


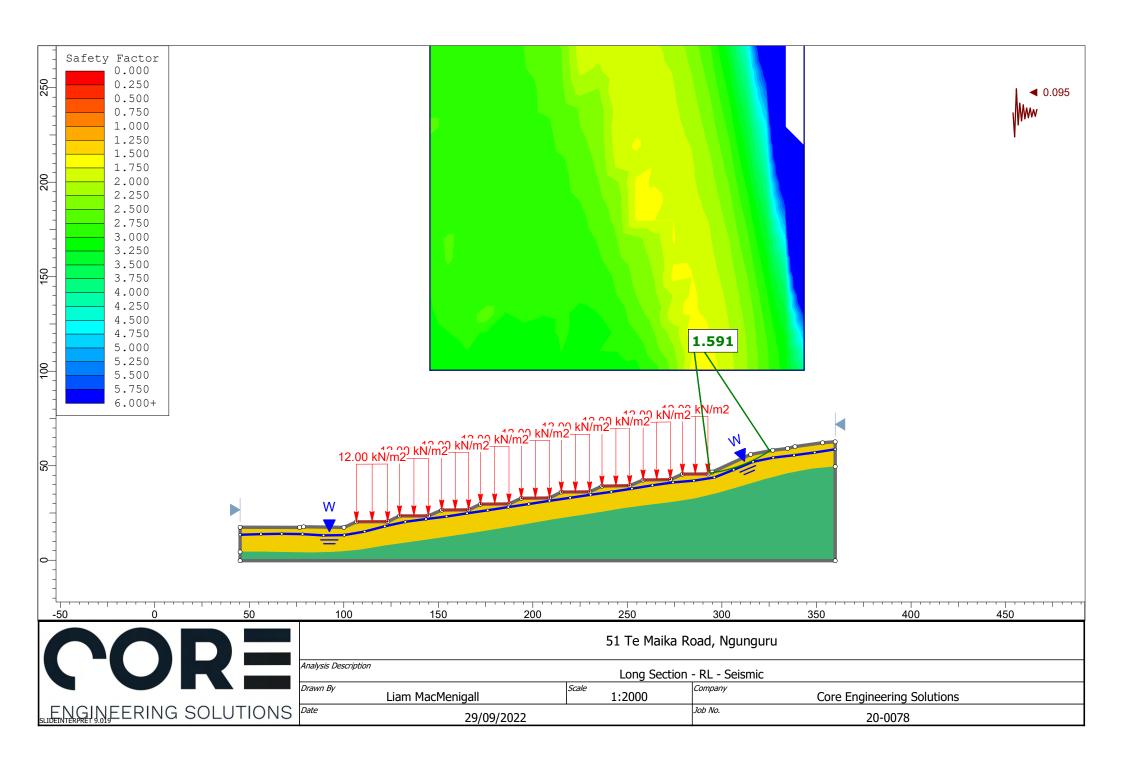














APPENDIX 8 - INSPECTION RECORDS

Job No: 20-0078



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			Consulting Engineers
CES JOB No. & REV.		INSPECTION No.	RET-004
ADDRESS			
INSPECTOR			
TYPE OF INSPECTION			
	CIVIL GEOTECHNICAL	STRUCTURAL	
CONSENT No.		DATE AND TIME	9 Dec 21 11.30am
H & S ISSUES ON SITE		H & S 'TAKE 5'	
		II & S TAKE S	
Cut complete for	r bottom retaining walls.		_
Good progress r	made on remaining walls, shear completed prior to Christmas.	r values continue hi	gh.
Bottom walls be	ing built after top walls.		
Bottom wans be	ing bant arter top wans.		
SITE CONTACT		COUNCIL INSPECTO	OR
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APPENDIX 9 – PRODUCER STATEMENTS FOR CONSTRUCTION FROM CONTRACTOR

Job No: 20-0078

NZS 3910:2013 Conditions of contract for building and civil engineering construction

Schedule 6 – Form of Producer Statement – Construction

ISSUED BY	Clements Contractors Ltd		(Contractor)
то	Traverse Ltd		(Principal)
IN RESPECT OF	Traverse Ltd - Te Maika Road Development		(Description of Contract Works)
AT	51 Te Maika Rd, Ngunguru, Whangarei		(Address)
	ctors Ltd (Contractor) has contracted to Traverse Ltd (Princ be with a Contract titled Traverse Ltd - Te Maika Road		
•	Ouly Authorised Agent) a duly authorised representative of Closs that Clements Contractors Ltd (Contractor) has carried		
All			
□ Part only as	s specified in the attached particulars of the contract work	s in accordance	with the Contract
Earthworks	S		
Rollinga	and		
T:	1.2	Date	3 August 2022
(Signature of Authorise	ed Agent on behalf of)		
Clements Contra	actors Ltd		
(Contractor)			
32 Westwood La	ne, Maunu		

NZS 3910:2013 Conditions of contract for building and civil engineering construction

Schedule 6 – Form of Producer Statement – Construction

ISSUED BY	Clements Contractors Ltd		(Contractor)
TO	Traverse Ltd		(Principal)
IN RESPECT OF	Traverse Ltd - Te Maika Road Development		(Description of Contract Works)
AT	<u> </u>		
AI	51 Te Maika Rd, Ngunguru, Whangarei		(Address)
	ctors Ltd (Contractor) has contracted to Traverse Ltd (P ce with a Contract titled Traverse Ltd – Te Maika Roa	•	
•	Duly Authorised Agent) a duly authorised representative of ds that Clements Contractors Ltd (Contractor) has carr		
☐ All			
□ Part only a	s specified in the attached particulars of the contract w	orks in accordance	with the Contract
	t and overlapping of Geo Composite material, and terial has been cut to install services	reinstatement to n	nanufacturers specification
Alleyn	and	Date	3 August 2022
(Signature of Authoris	eed Agent on behalf of)		
Clements Contr	actors Ltd		
(Contractor)			
32 Westwood L	ane, Maunu		
(Address)			

NZS 3910:2013 Conditions of contract for building and civil engineering construction

Schedule 6 – Form of Producer Statement – Construction

ISSUED BY	Clements Contractors Ltd	(Contractor)
то	Traverse Ltd	(Principal)
IN RESPECT OF	Traverse Ltd - Te Maika Road Development	(Description of Contract Works)
AT	51 Te Maika Rd, Ngunguru, Whangarei	(Address)
	ctors Ltd (Contractor) has contracted to Traverse Ltd (Principle with a Contract titled Traverse Ltd – Te Maika Road I	
Ryan Hayward (£	Ouly Authorised Agent) a duly authorised representative of Cle	ements Contractors Ltd (Contractor) believe on
reasonable ground	s that Clements Contractors Ltd (Contractor) has carried	out and completed:
☐ AII		
□ Part only as	s specified in the attached particulars of the contract work	ks in accordance with the Contract
Retaining \	Walls	
Rollinga	and	
		Date 3 August 2022
(Signature of Authorise	ed Agent on behalf of)	
Clements Contra	actors Ltd	
(Contractor)		

SIXTH SCHEDULE

FORM OF PRODUCER STATEMENT - CONSTRUCTION

ISSUED BY: Webb Contracting Ltd (Contractor) TO: Traverse LTD - Clements Contractors (Principal) TO BE SUPPLIED TO: Whangarei District Council (Territorial authority) IN RESPECT OF: 51 Te Maika Road DP374000 (Description of Contract Works) AT: 51 Te Maika Road, Ngunguru, Whangarei. (Address) Webb Contracting Ltd (Contractor) has contracted to Traverse Limited (Principal) to carry out and complete certain building works in accordance with a contract, titled Traverse - Lot 51 Te Maika Road ("the contract") I Jake Pattison (Duly Authorized Agent) a duly authorized representative of Webb Contracting Ltd (Contractor) believe on reasonable grounds that Webb Contracting Ltd (Contractor) has carried out and completed ΑII Part only as specified in the attached particulars of the building works in accordance with the contract. Laying of Ø1350mm Stormwater line Lance Smith - Certifying Drainlayer #20798 Date 2nd August 2022 (Signature of Authorized Agent on behalf of) Webb Contracting Ltd (Contractor) 247 Three Mile Bush Road, Kamo, Whangarei 0145 (Address)